

Formalizing Hybrid Systems with Event-B

Jean-Raymond Abrial, Wen Su, Huibiao Zhu

August 2012

Prologue

Using B Formal Method in Industry

- Fully automatic train systems:
 - Paris metro line 14 (October 1998)
 - Roissy airport shuttle (March 2007)
- More train applications

Line length	8.5 km
Number of Stops	8
Time interval between two trains	115 s
Speed	40 km/h
Number of trains	17
Passengers per day	350,000

Line length	3.3 km
Number of Stops	5
Time interval between two trains	105 s
Speed	26 km/h
Number of trains	14
Passengers per hour	2,000

	Paris	Roissy
Number of final ADA lines (from B)	86,000	158,000
Number of proofs	27,800	43,610
Percentage of interactive proofs	8.1	3.3
Interactive proofs in Man.Month	7.1	4.6

- Man.month calculated with:
 - 15 interactive proofs per man.day
 - 21 days in a month
- In both cases, no unit tests and no integration tests
- Reinforcing global tests (catastrophic scenarios)
- Important differences in the software requirements:
 - Paris: specially done for the project
 - Paris: adaptation from O'Hare Airport (problems)

City	Line	Service	Driverless
Algiers	1	2011	No
Barcelona	9	2007	Yes
Budapest	4	2013	Yes
Caracas	4	2004	No
Helsinki	1	2013	No
Hong Kong	TKO	2001	No

City	Line	Service	Driverless
Mexico	B	2000	No
New York	Canarsie	2006	No
	PATH	2014	No
Paris	14	1998	Yes
	3	2009	No
	1	2011	Yes
	5	2012	No

City	Line	Service	Driverless
Rennes	B	2018	Yes
Roissy CDG	1	2007	Yes
	2	2007	Yes
San Juan	2	2004	No
Sao Paulo	TKO	2001	Yes

Contact: <Jean-Marc.Meynadier@siemens.com>

System	City	Service	Size	Language	Driverless
KVB	French Trains	1993	30000	ADA	No
CDTC	Cairo	1996	3000	Modula2	No
SACEM	Paris (RER B)	1996	2500	Modula2	No
ACSES	AMTRACK (USA)	2002	14500	ADA	No

System	City	Service	Size	Language	Driverless
Urbalis 200	Shanghai	2003	30000	ADA	No
	New Dehli				
	Seoul				
	Daegu				
	Incheoun				
	Madrid				
	Santiago	2013			
	Cairo				
	Bangalore				
	Calcutta				

System	City	Service	Size	Language	Driverless
Urbalis 400	Shanghai	2008	100000	ADA	No
	Beijing				Yes
	Chenzen				No
	Sao Paulo	2013			Yes
	Mexico				No
	Milano				No
	Toronto				No
	Wuhan				No

Contact: <Luis-Fernando.Mejia@transport.alstom.com>

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- BUT, when introducing such continuous transitions
the **discrete** transitions are **still needed**
- Hence the notion of **hybrid systems**
where **both** discrete and continuous transitions can occur

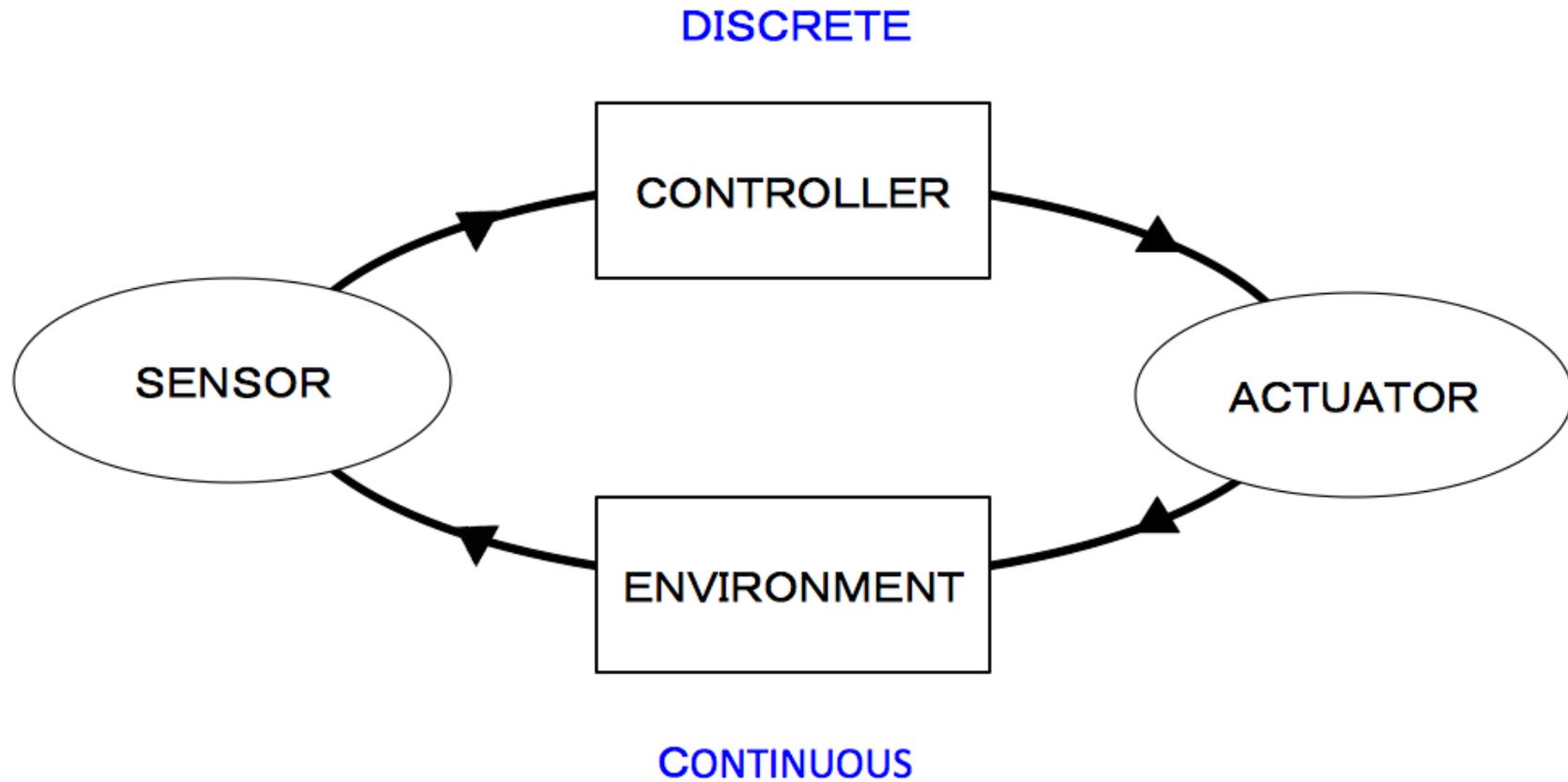
- Hybrid frameworks are frequent in embedded systems where:

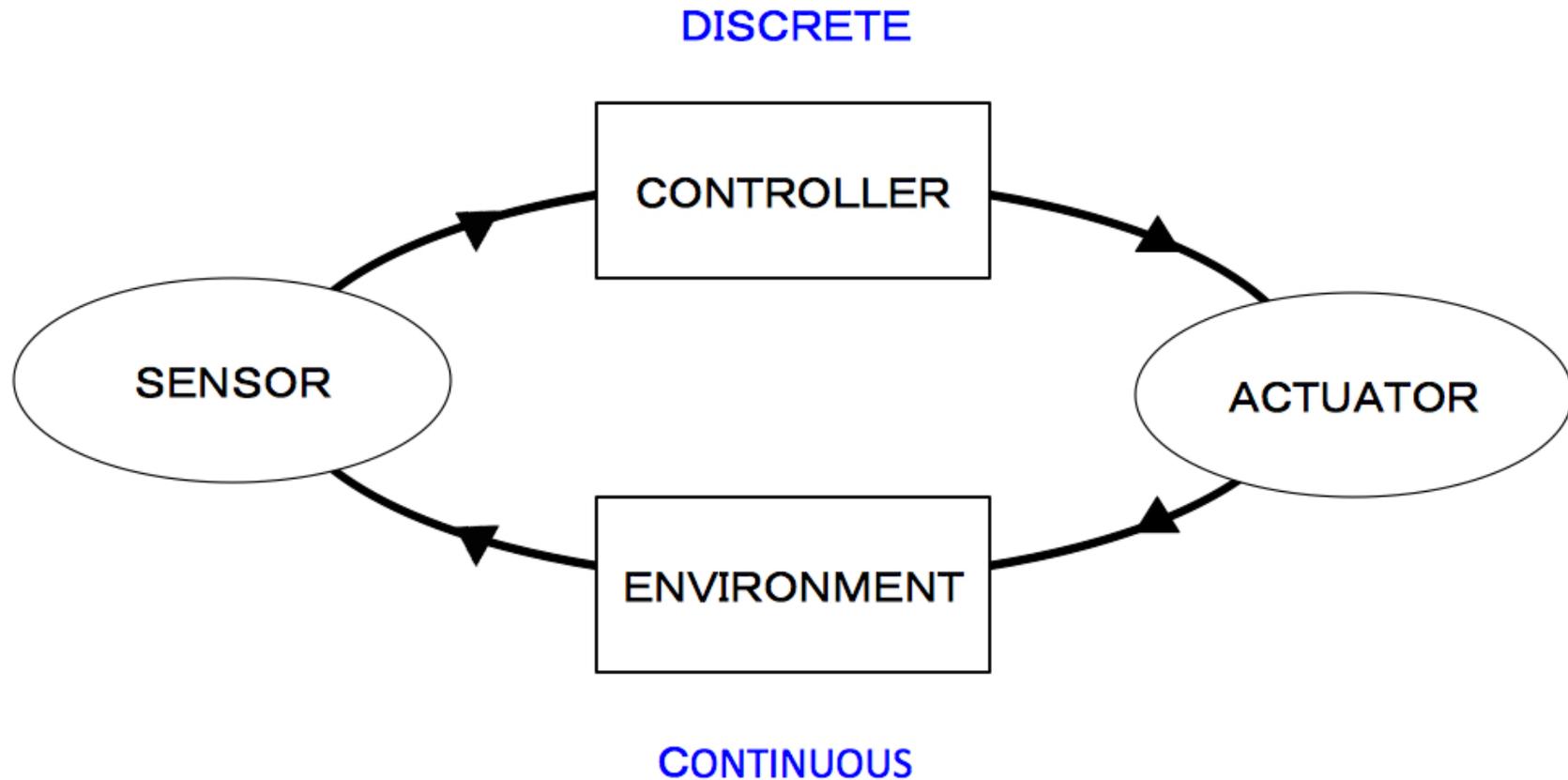
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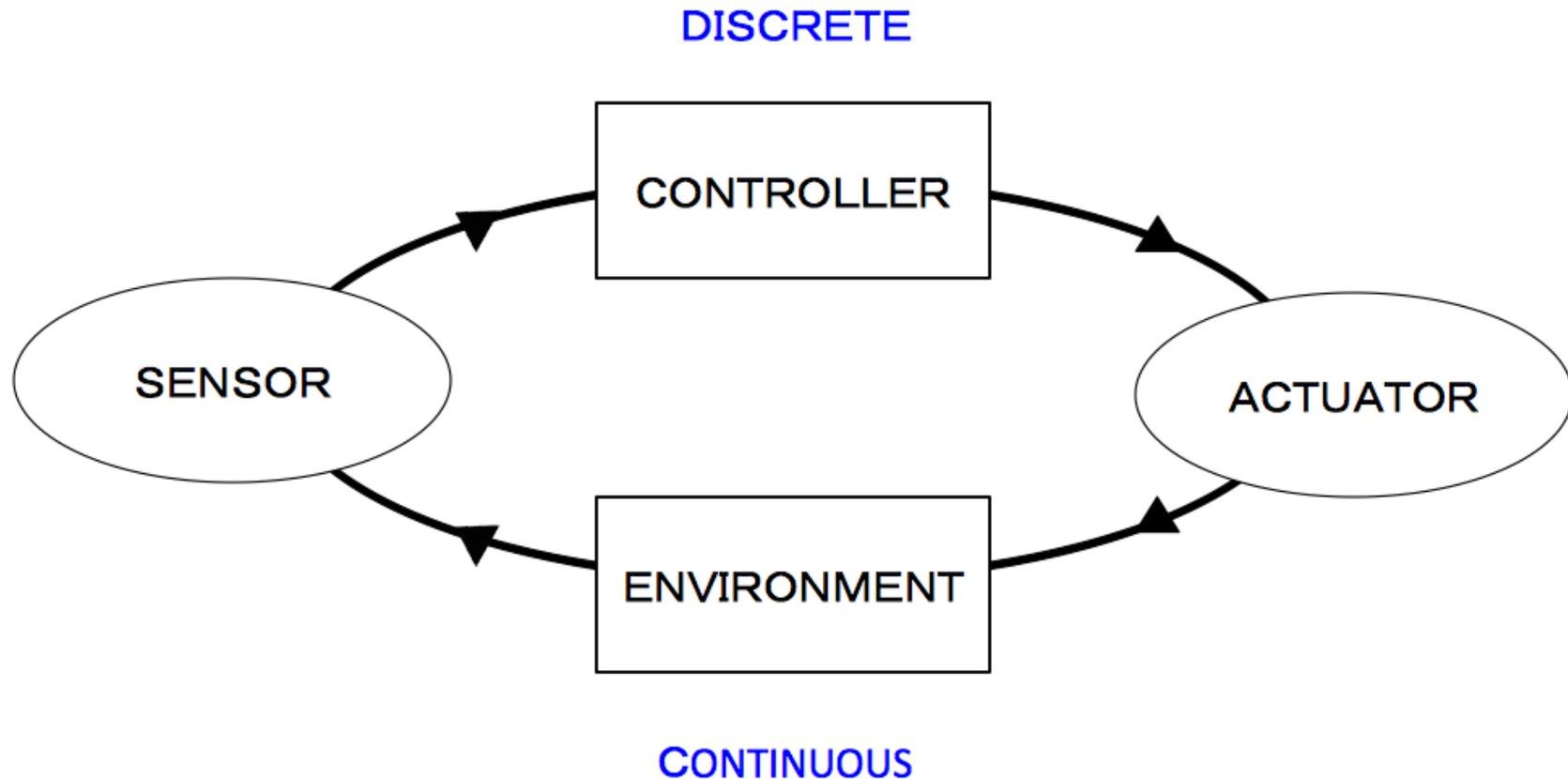
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- **Hybrid frameworks** are frequent in **embedded systems** where:
 - A piece of software, the **controller**, manages an **environment**
 - **Controller** is linked to **environment** by **sensors** and **actuators**
 - Controller works from time to time in a **DISCRETE** fashion
 - While environment evolves in a **CONTINUOUS** way.





- We want to develop **models** of such **closed systems**



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- We have thus to cope with both **discrete** and **continuous** evolutions

- **Continuous** physical environment:
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- **Goal**: to control the **speed** of the train (station or another train)

R.J. Back and R. Kurki-Suonio.

Distributed Cooperation with Action Systems

ACM Transaction on Programming Languages and Systems. 1988.

R.J. Back, L. Petre, and I. Porres.

Generalizing Action Systems to Hybrid Systems.

FTRTFT 2000. LNCS 1926 Springer Verlag, 2000.

R.J. Back, C. Cerschi Seceleanu, and J. Westerholm.

Symbolic Simulation of Hybrid Systems.

APSEC'02, 2002.

Formalizing Hybrid Systems with Event-B

ABZ Conference. Pisa, June 2012

Complementary Methodologies for Developing Hybrid Systems with Event-B

Accepted at ICFEM 2012. Kyoto, November 2012

- Discrete variables together with continuous variables

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- We are interested in the immediate future of continuous variables
- Discrete systems as an abstraction of continuous ones
- We thus use refinement from a discrete to a continuous system

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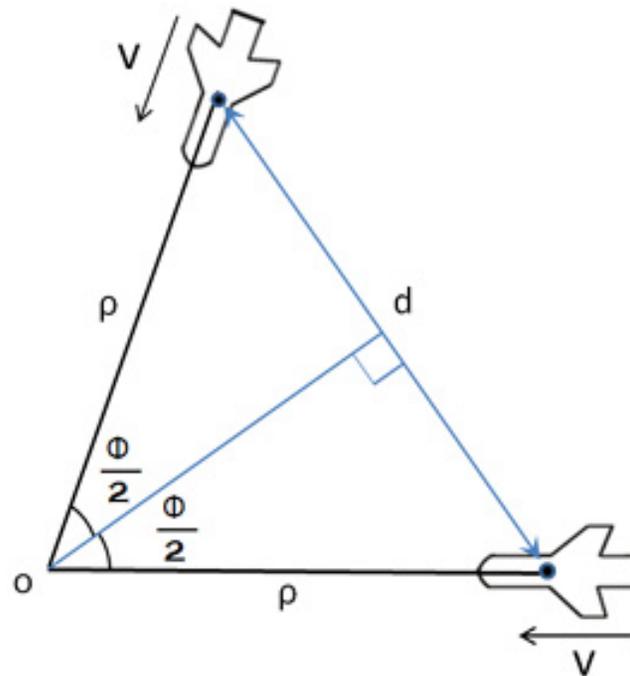
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 - Examples developed and **fully proved** with the **Rodin Platform**
 - These examples show complete **analytical solutions**

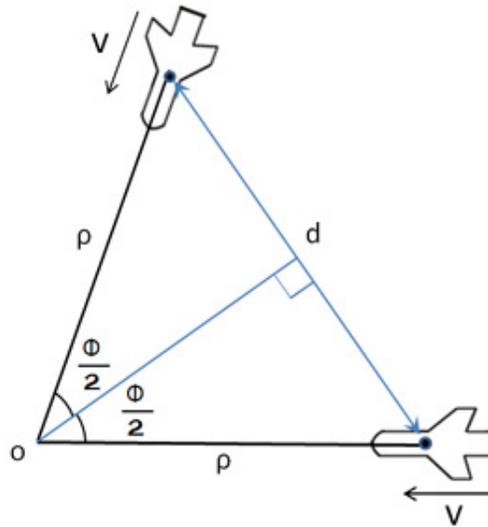
Example 1

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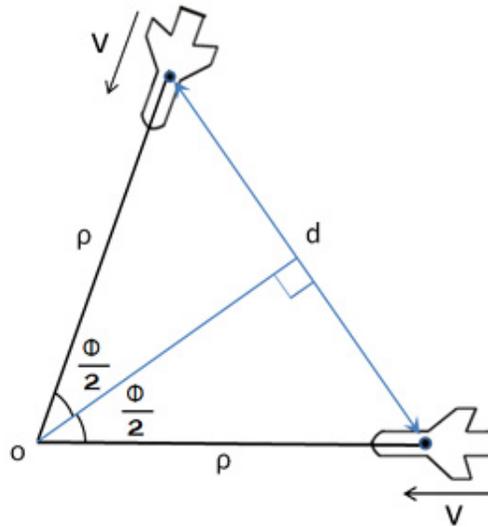
- Two aircraft are flying at the **same altitude** and **speed**
- They might **converge** (collision) at some point o





- The **distance** between aircrafts is as follows:

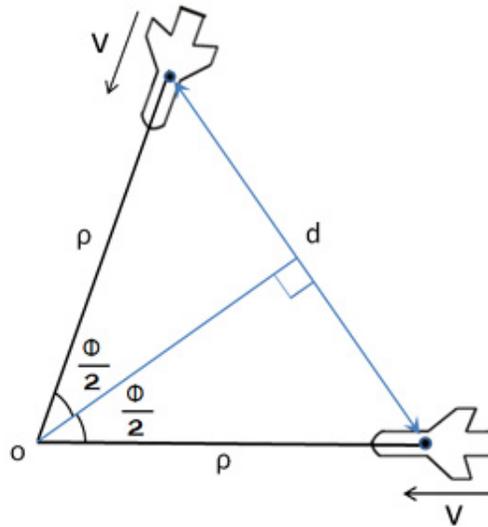
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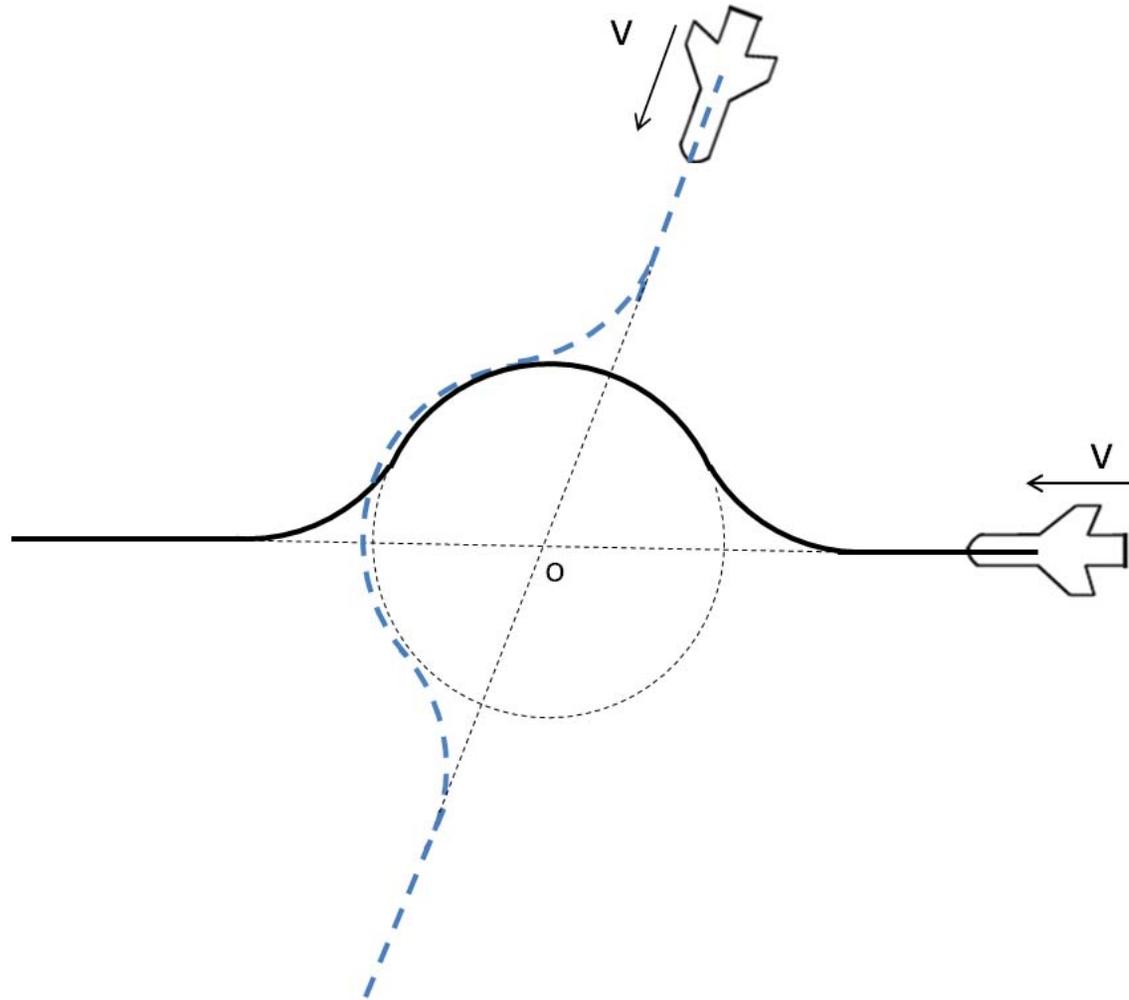
- Their **distance** must always be **greater than or equal to** a constant p



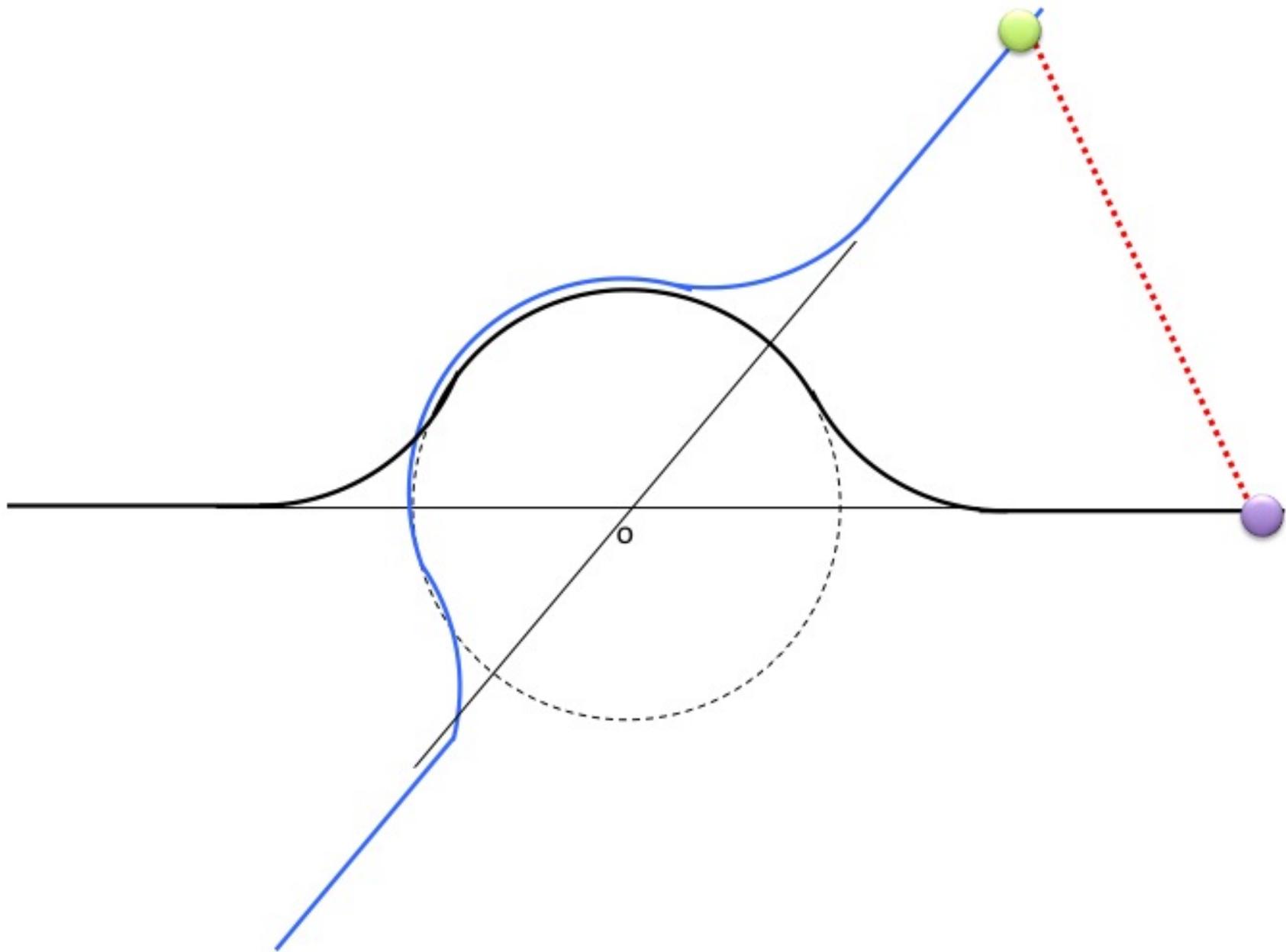
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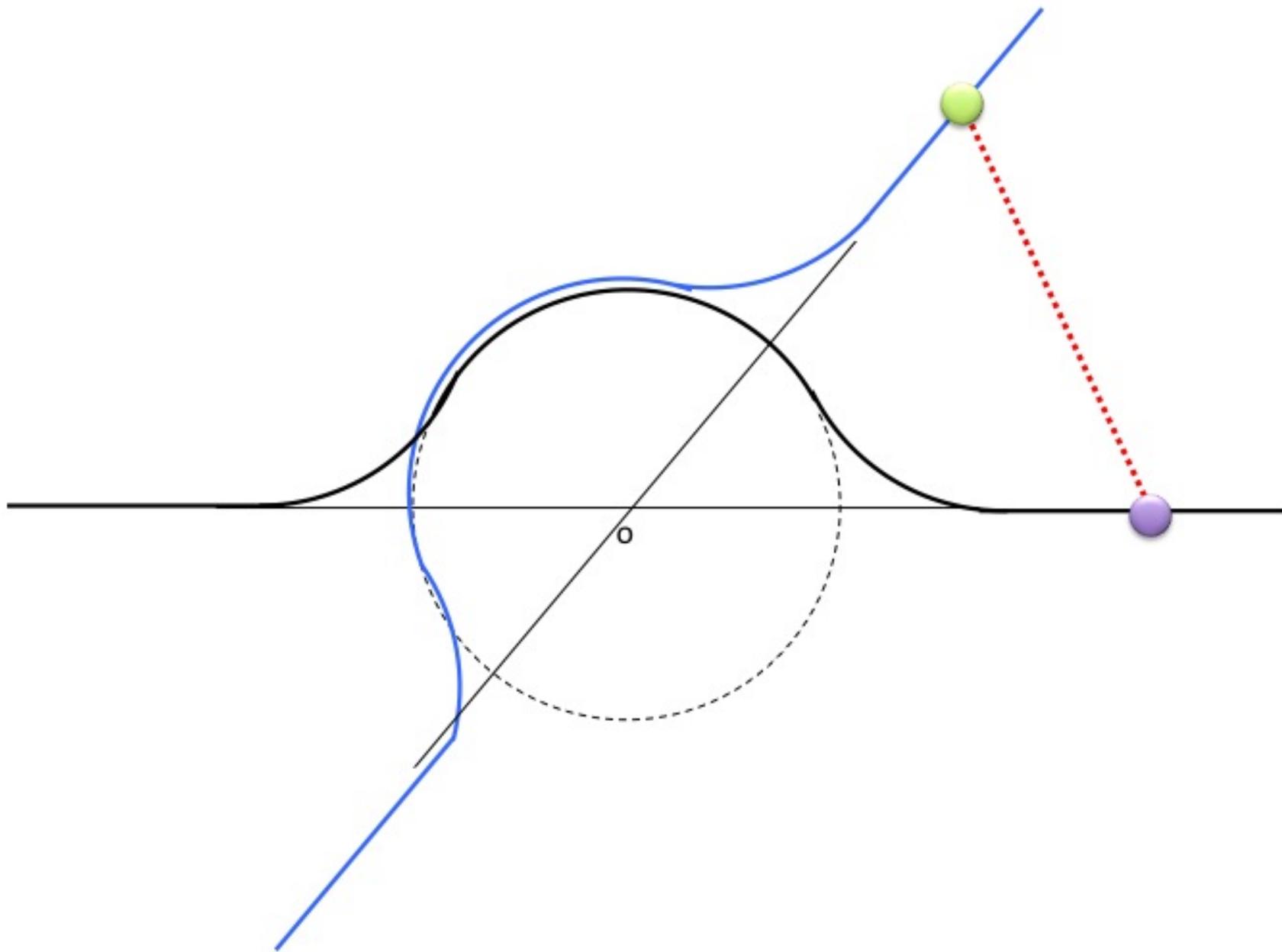
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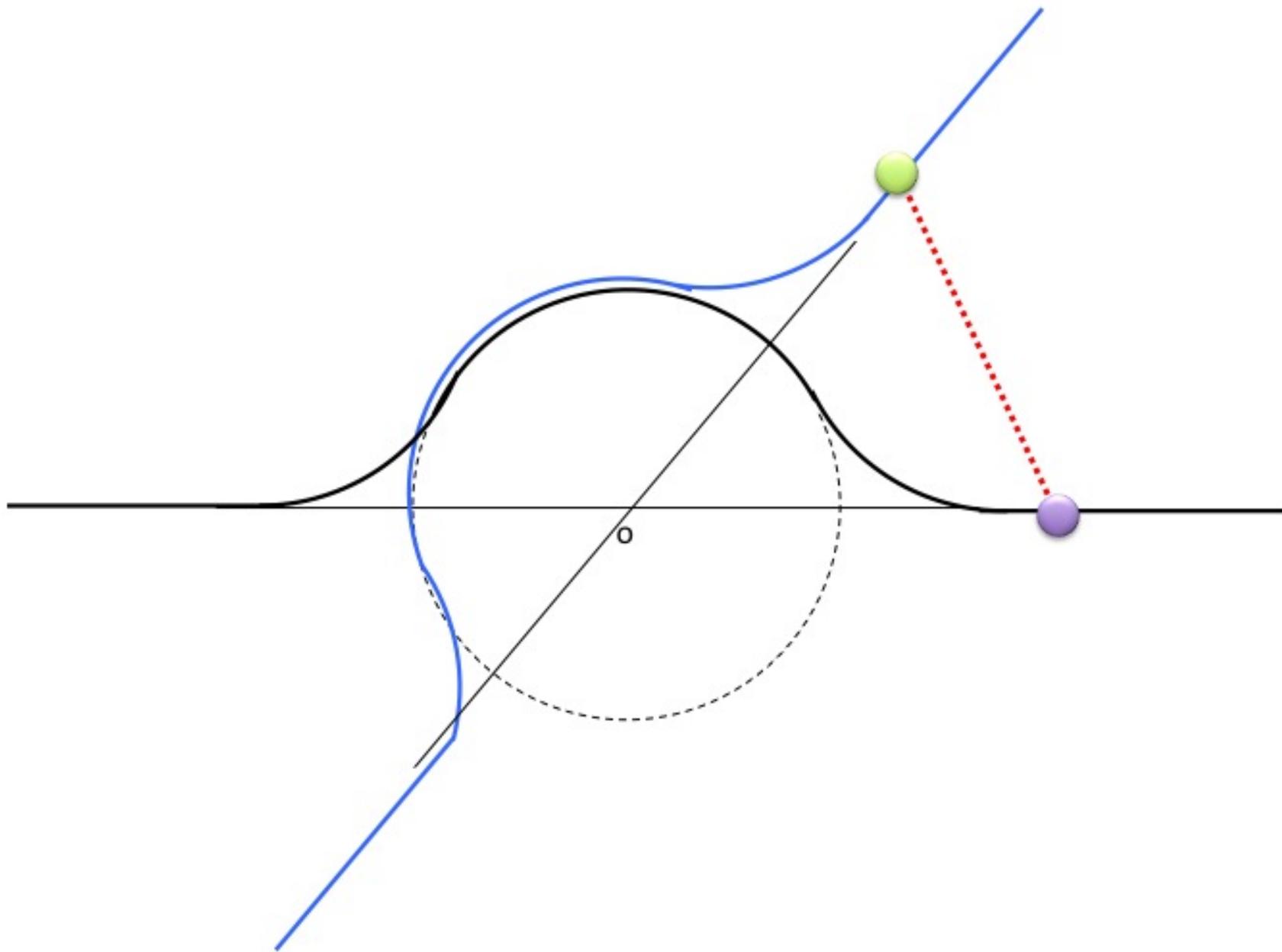
- Their **distance** must always be **greater than or equal to** a constant p
- **Goal**: we want to find a solution to **avoid** the **collision**

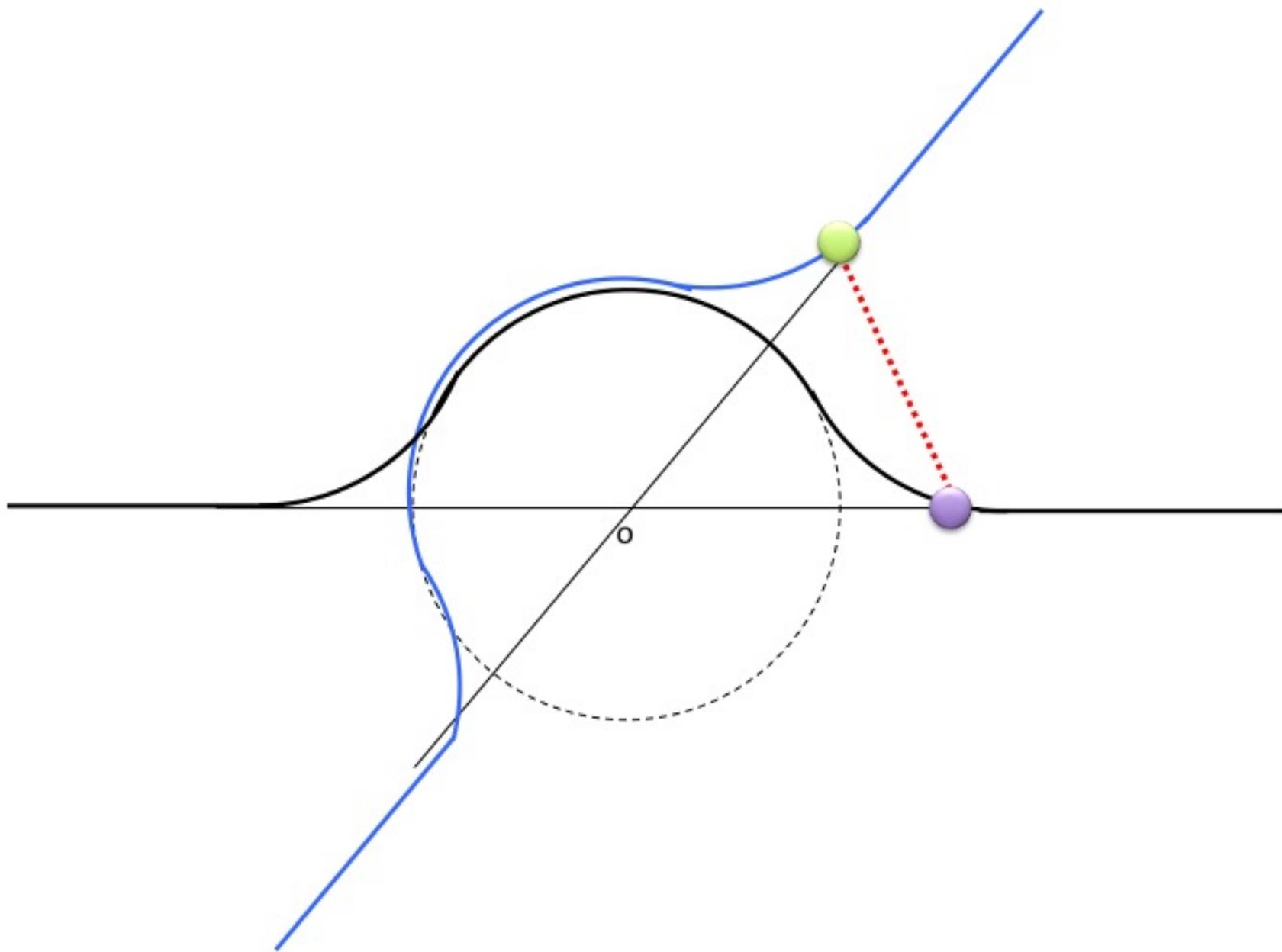


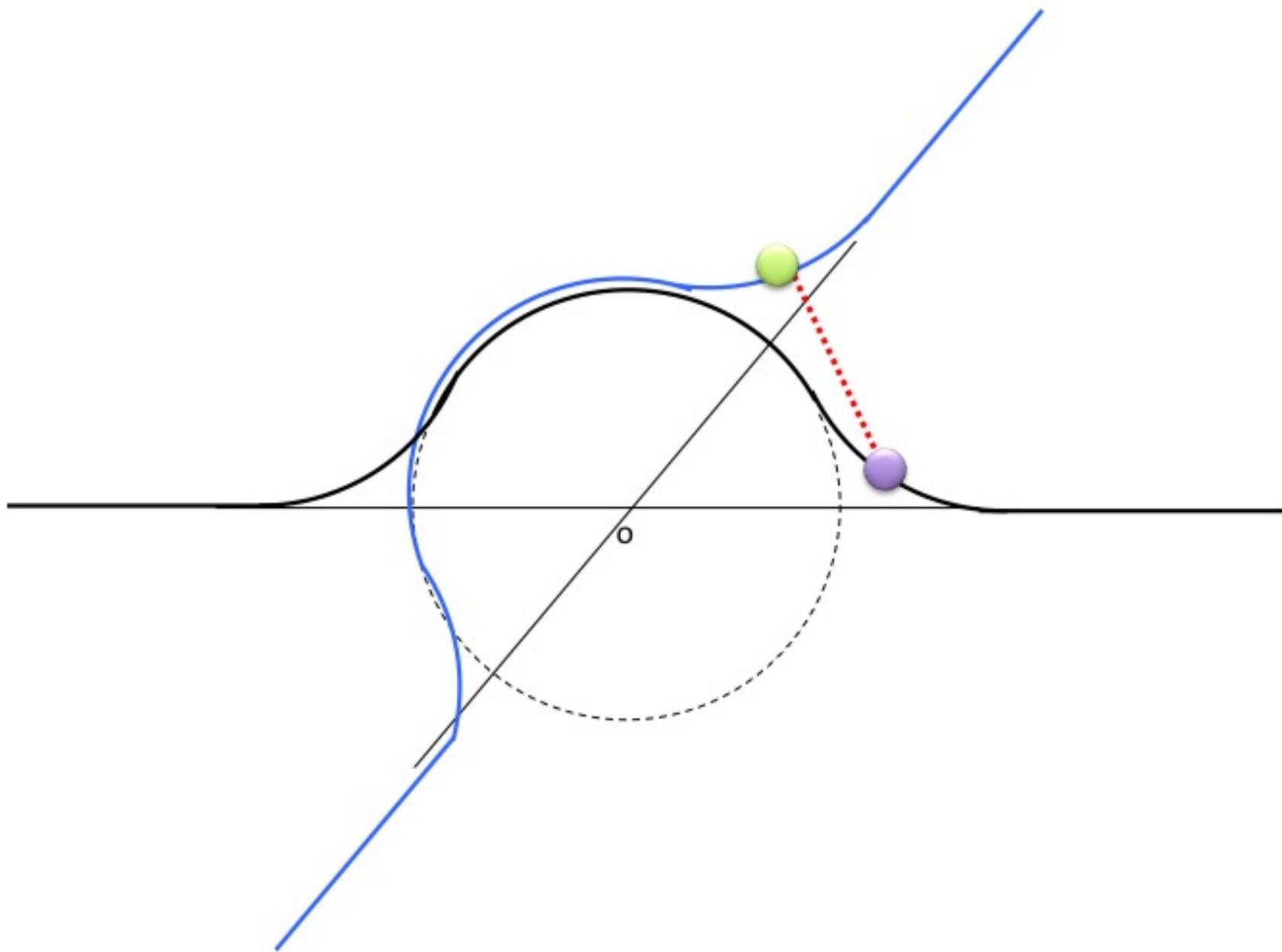
- The **radius r** of this circle will be determined later
- **Both aircrafts** continue to **fly** at the **same speed** during the maneuver

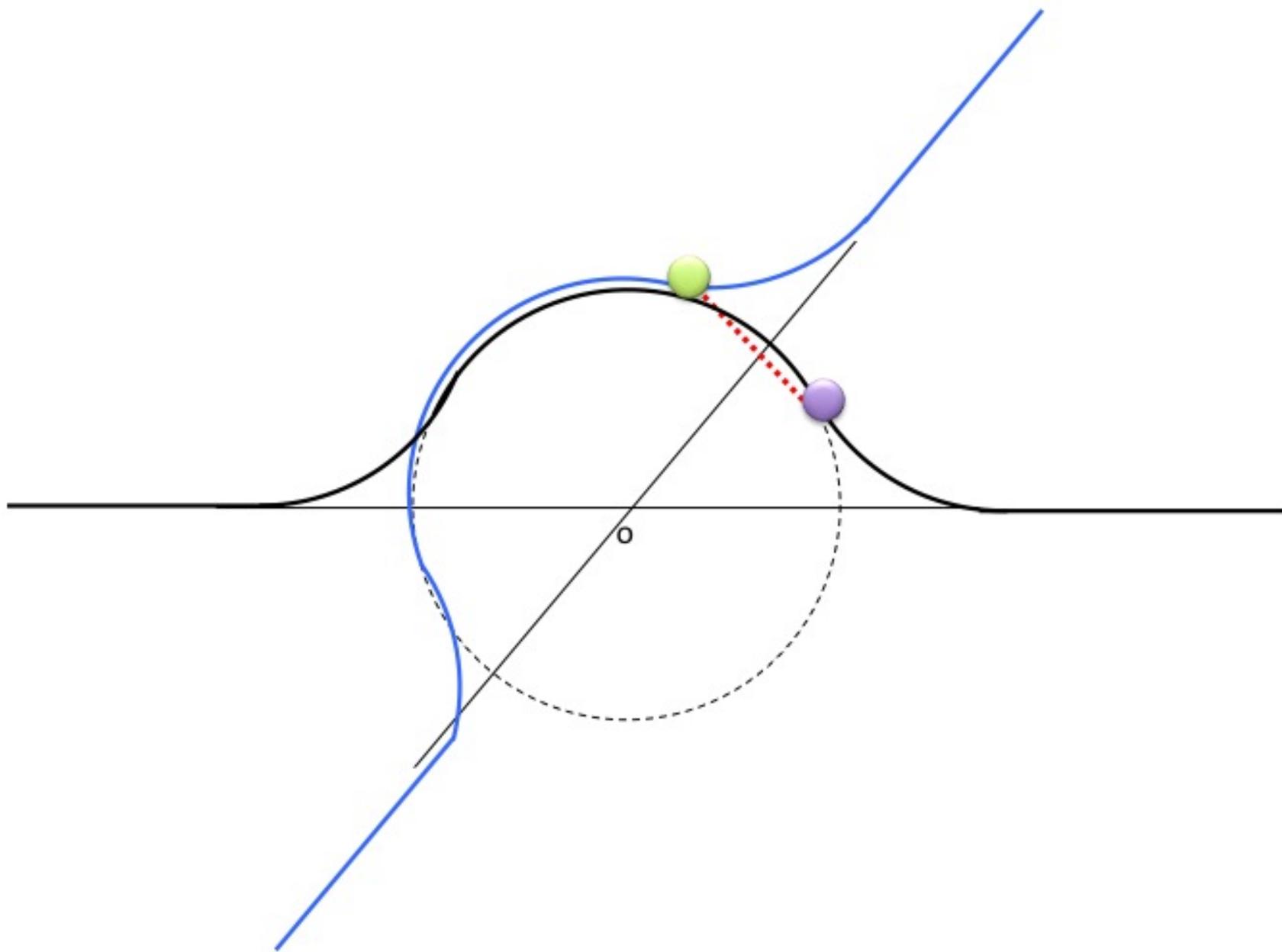


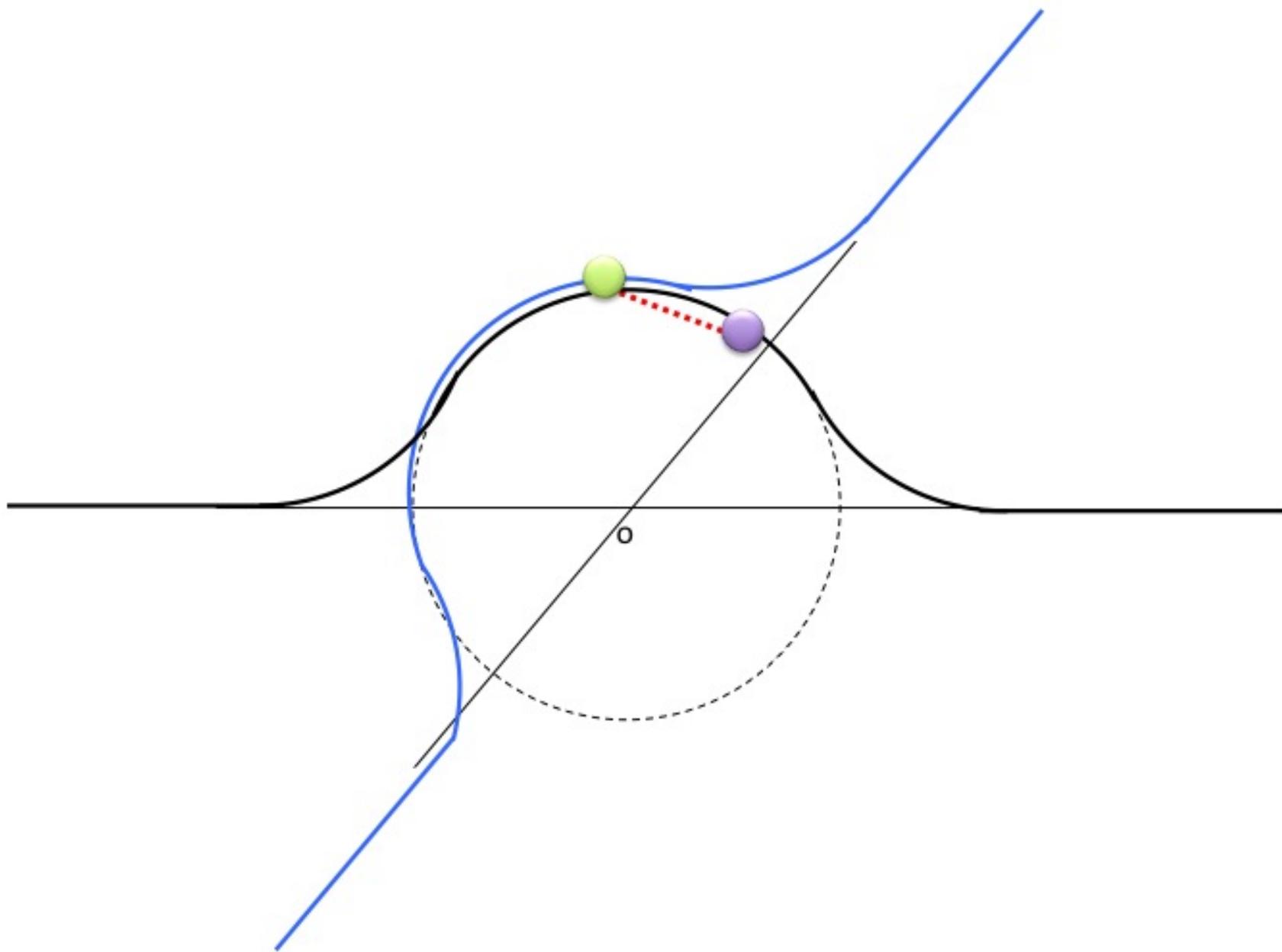


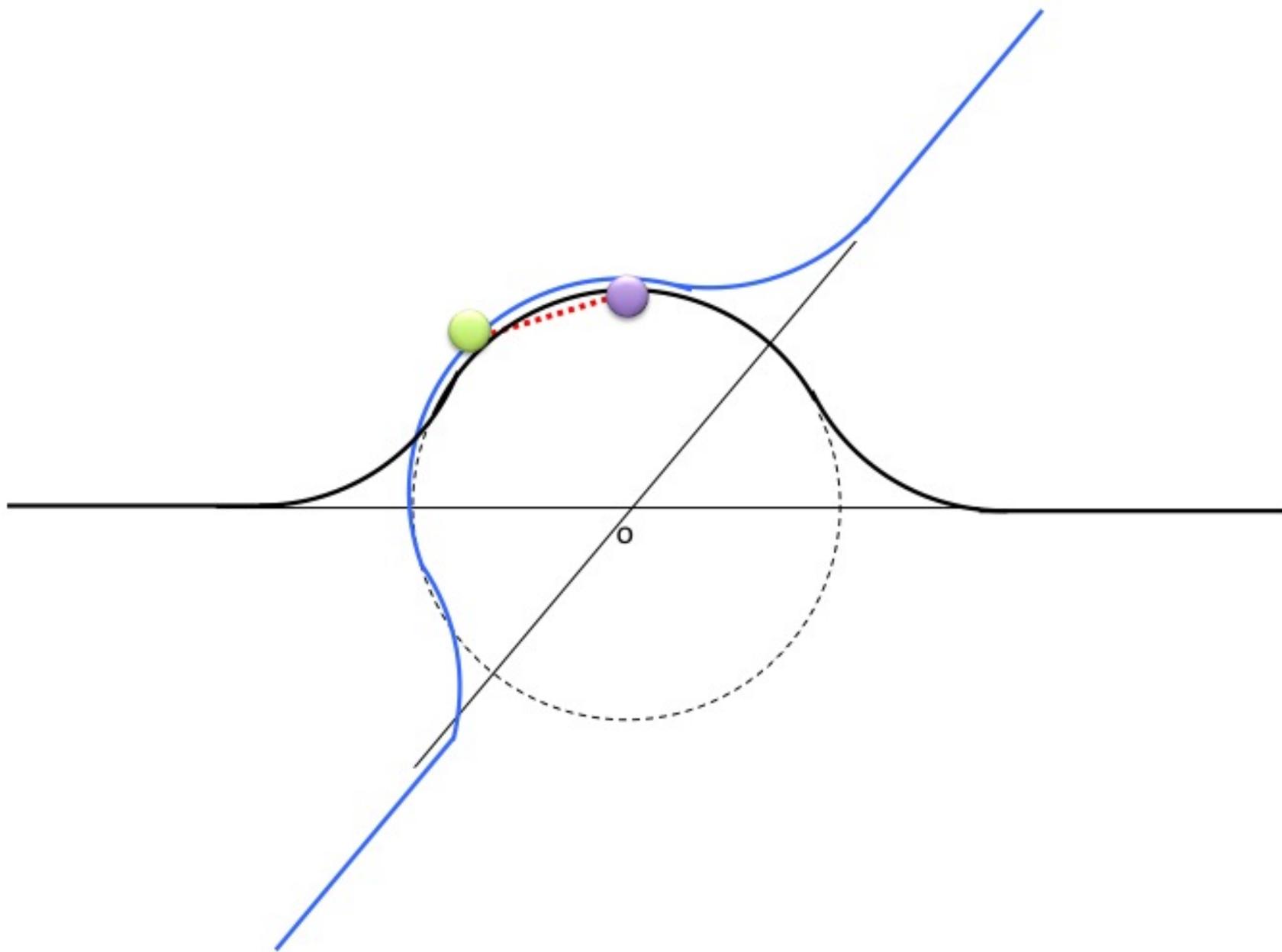


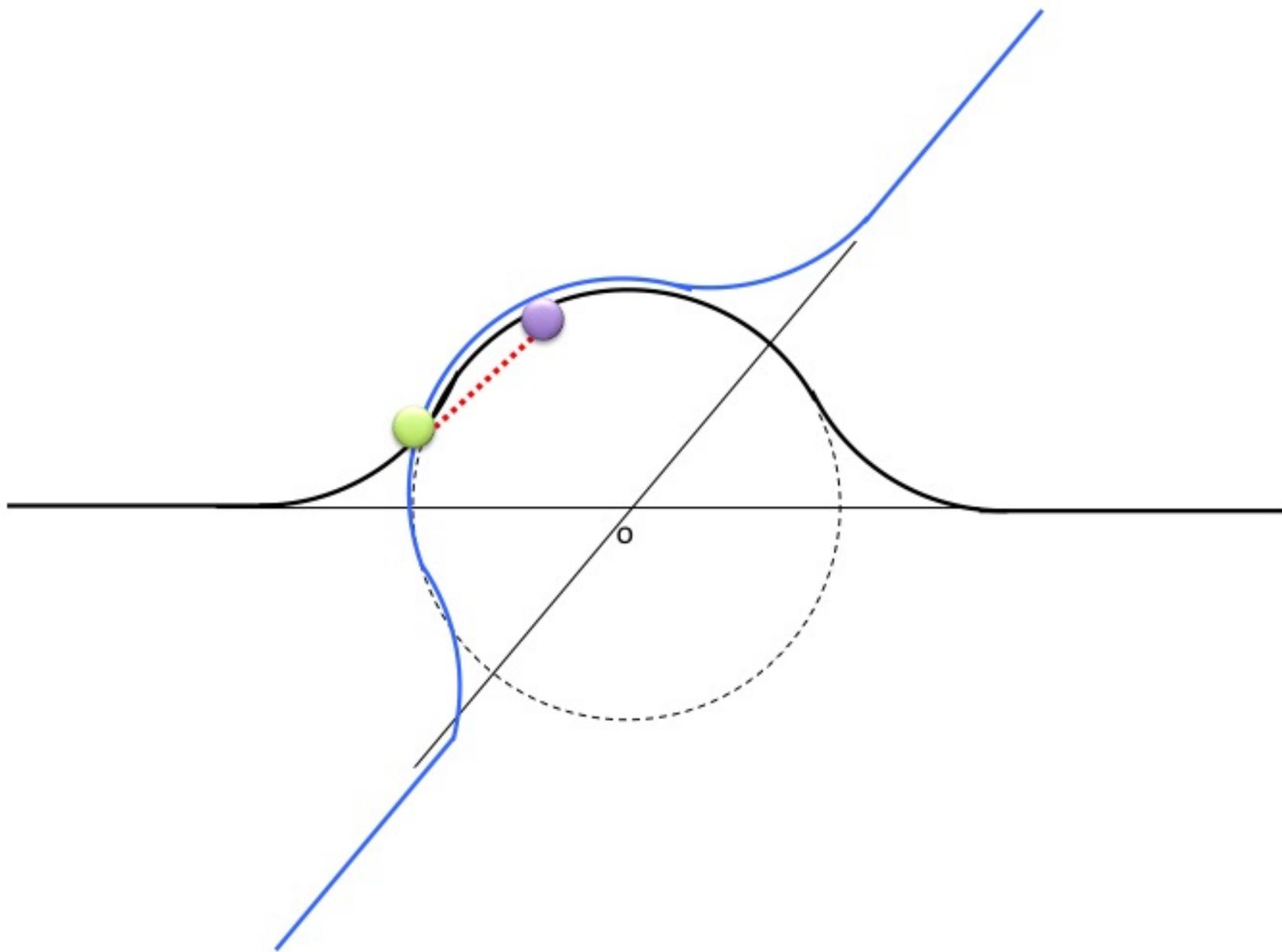


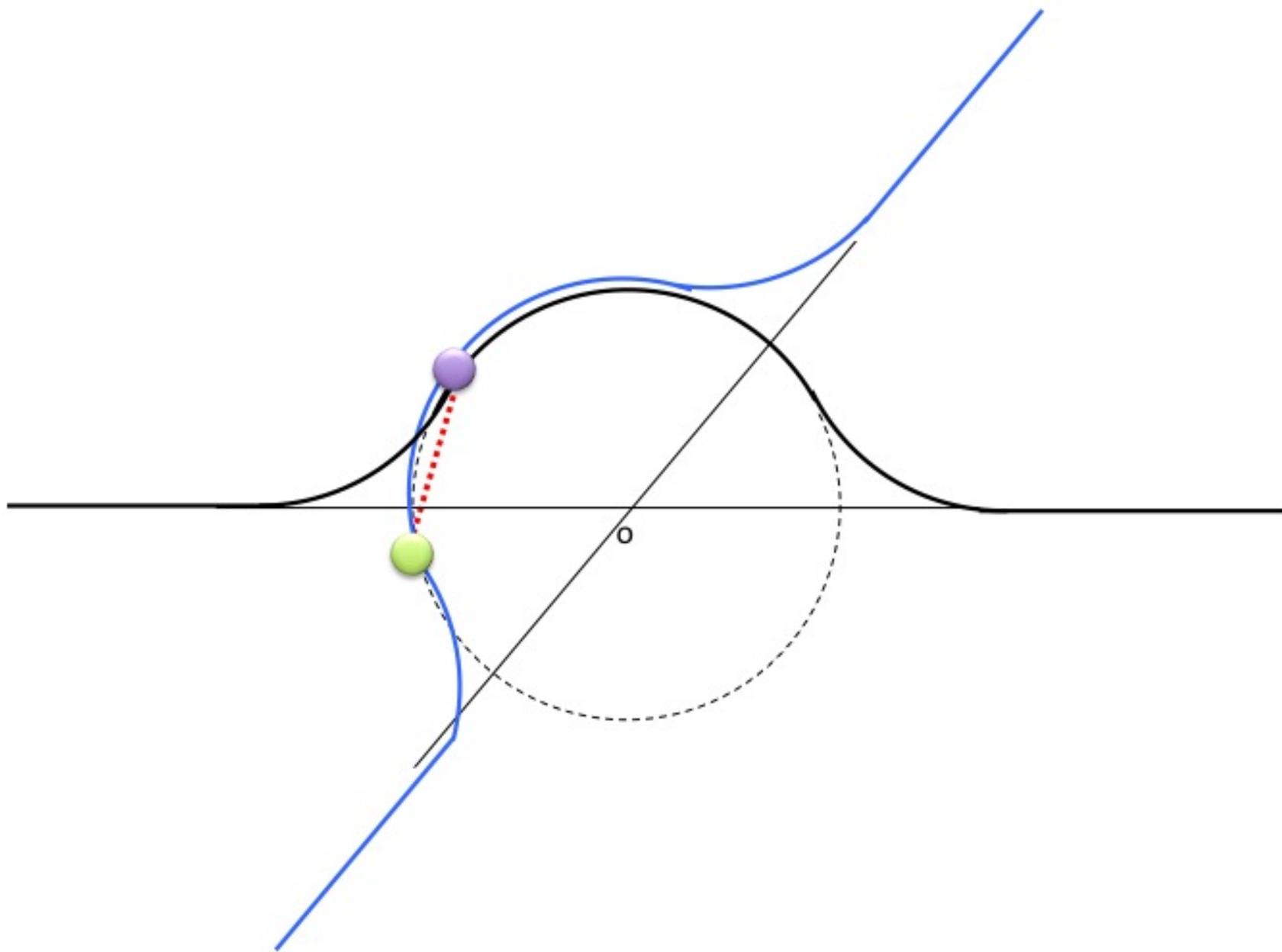


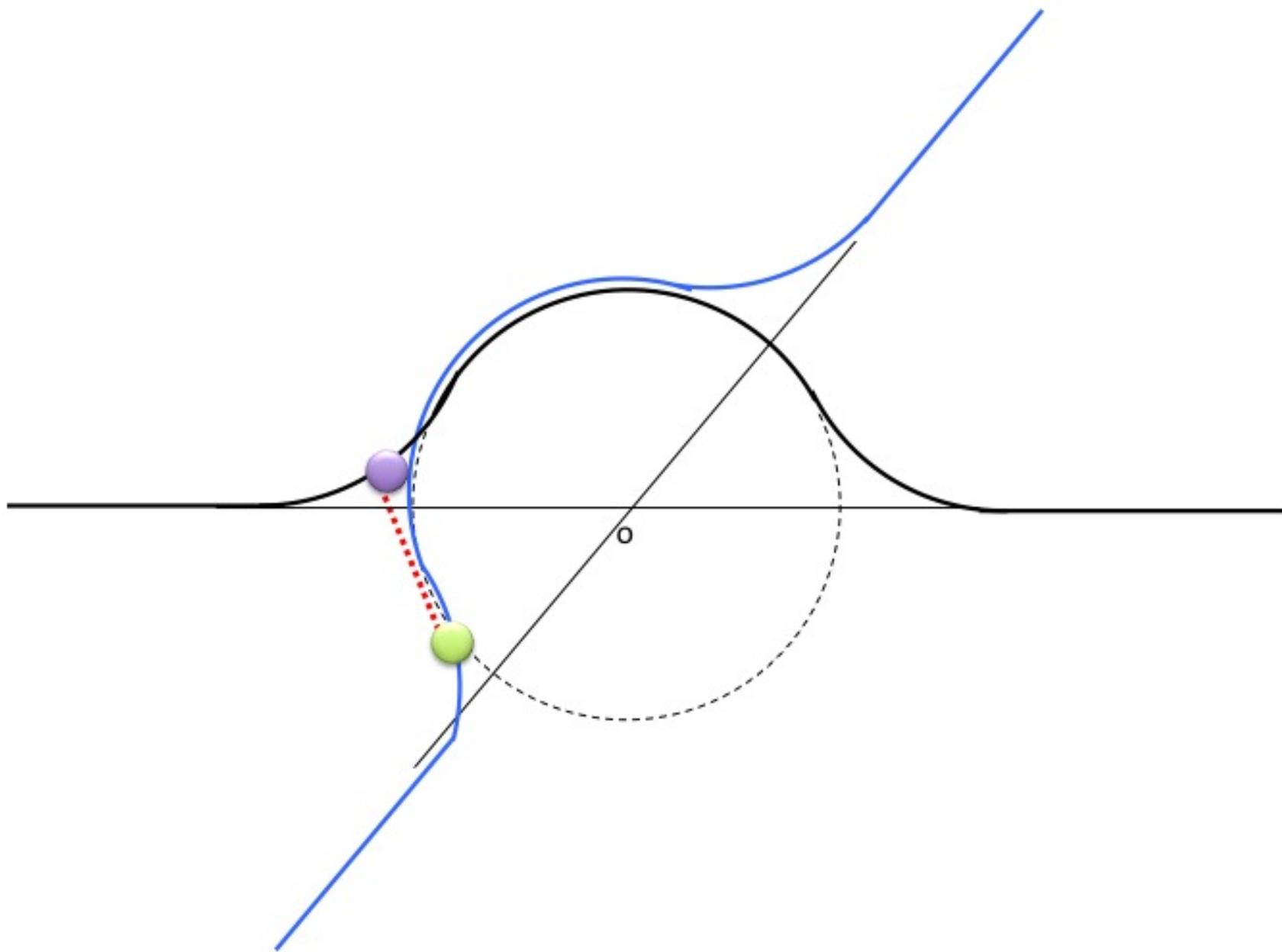


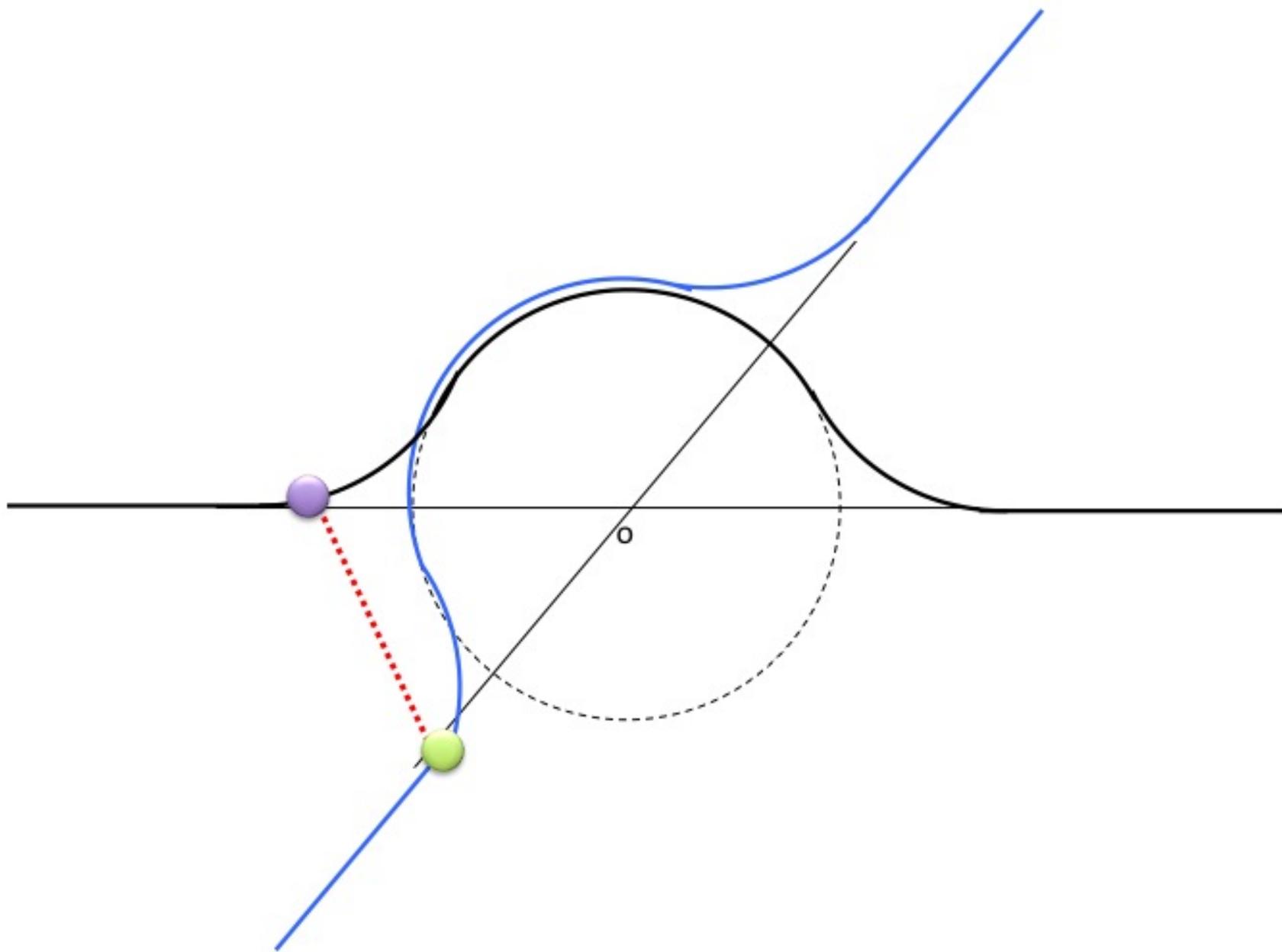


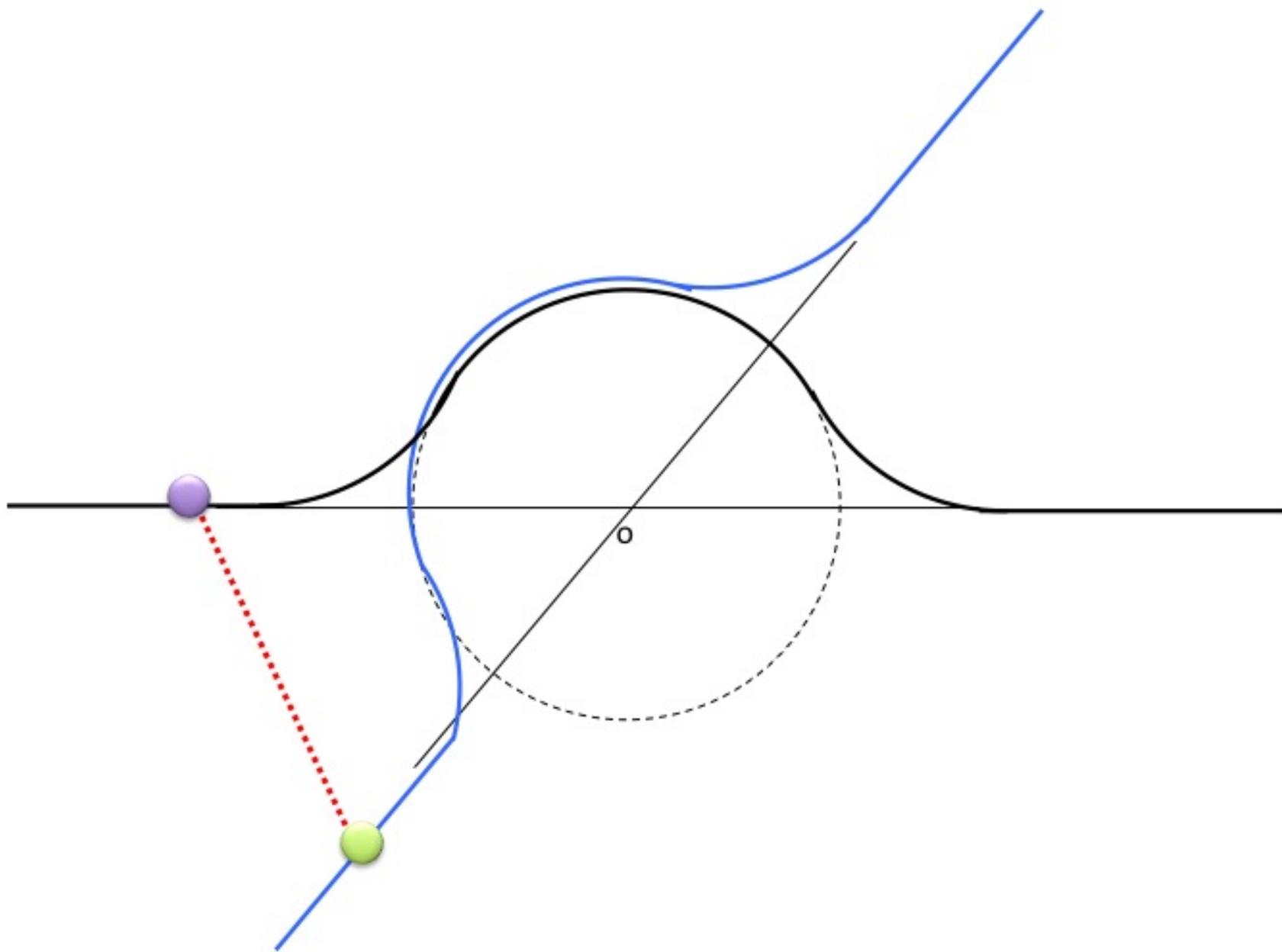


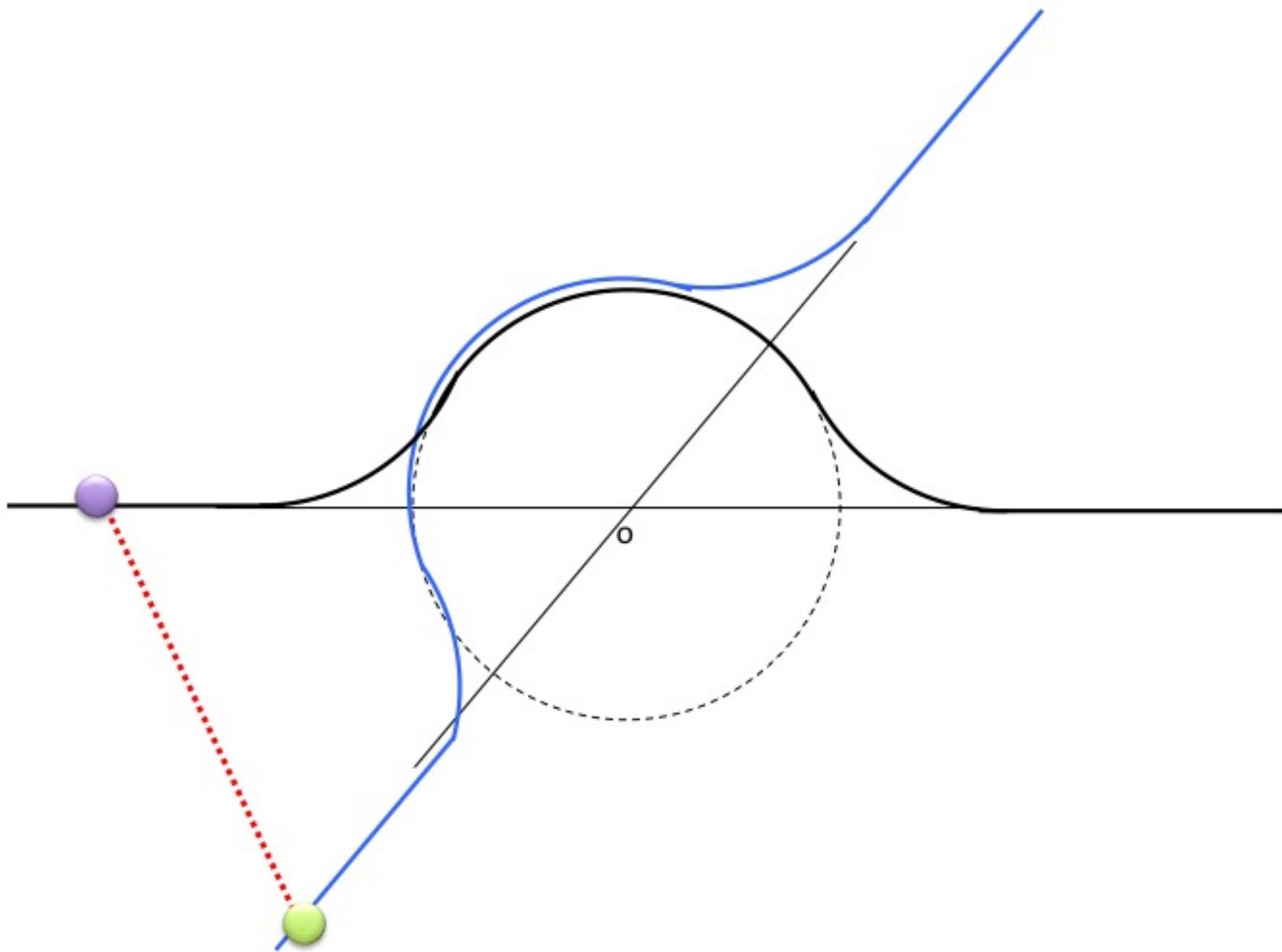












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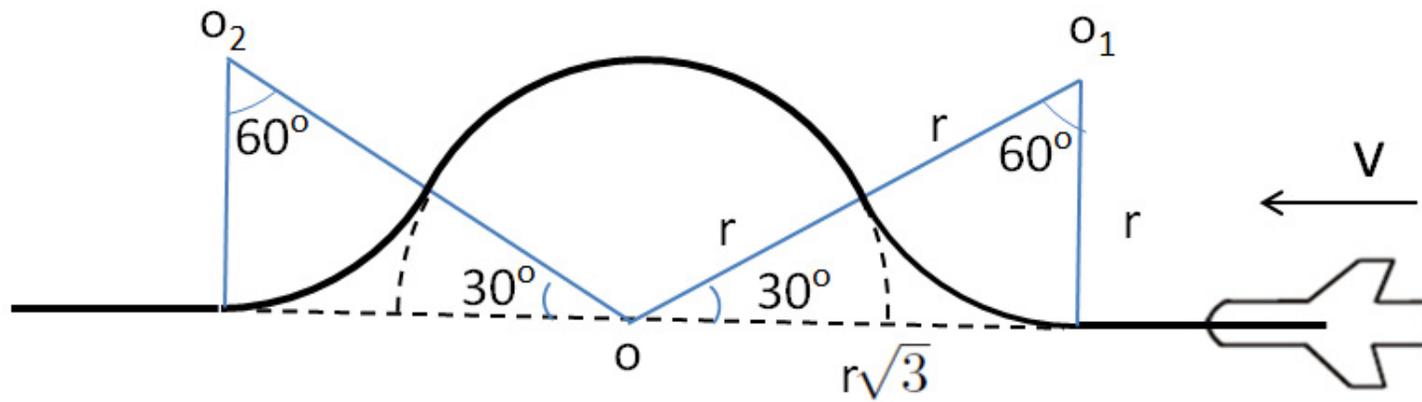
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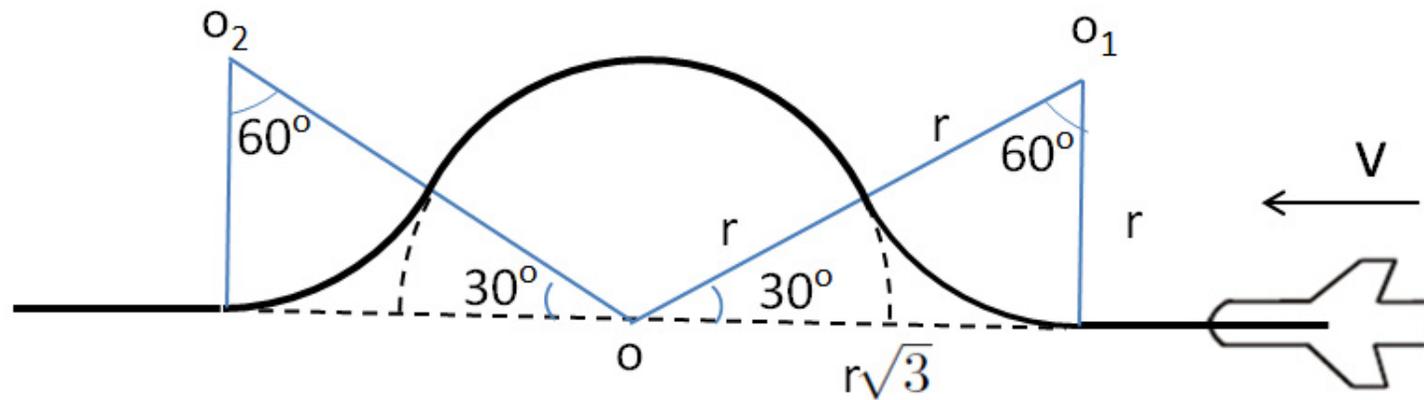
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- Angle ϕ between aircrafts **does not change** during the maneuver
- **Both aircrafts** are still at the **same distance r** of the point o
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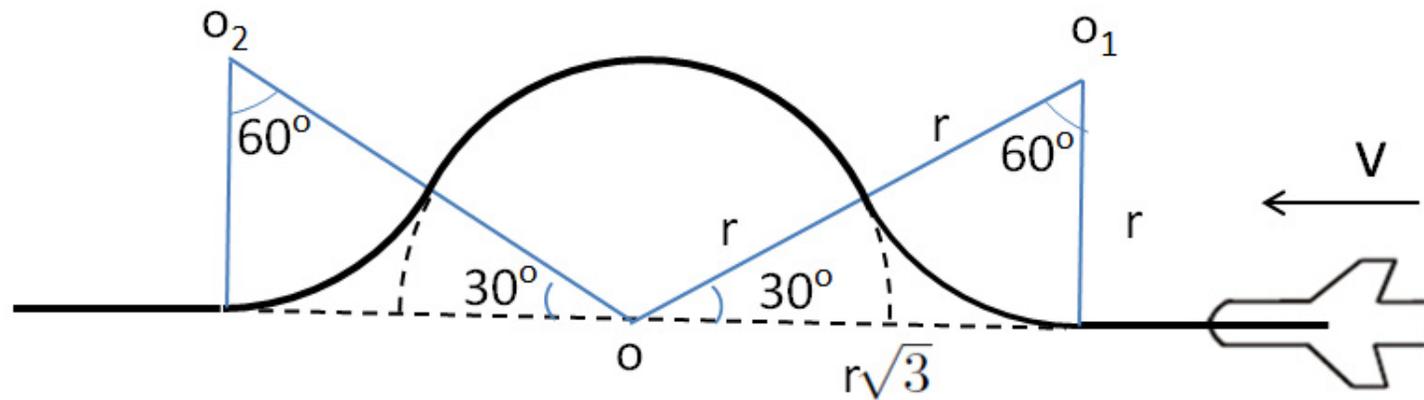
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- is the **common distance ρ** of both aircrafts to the collision point o
- The **smallest distance** is when they are **on the circle** (more later)
- We must have then: $\frac{p}{2 \sin \frac{\phi}{2}} \leq r$

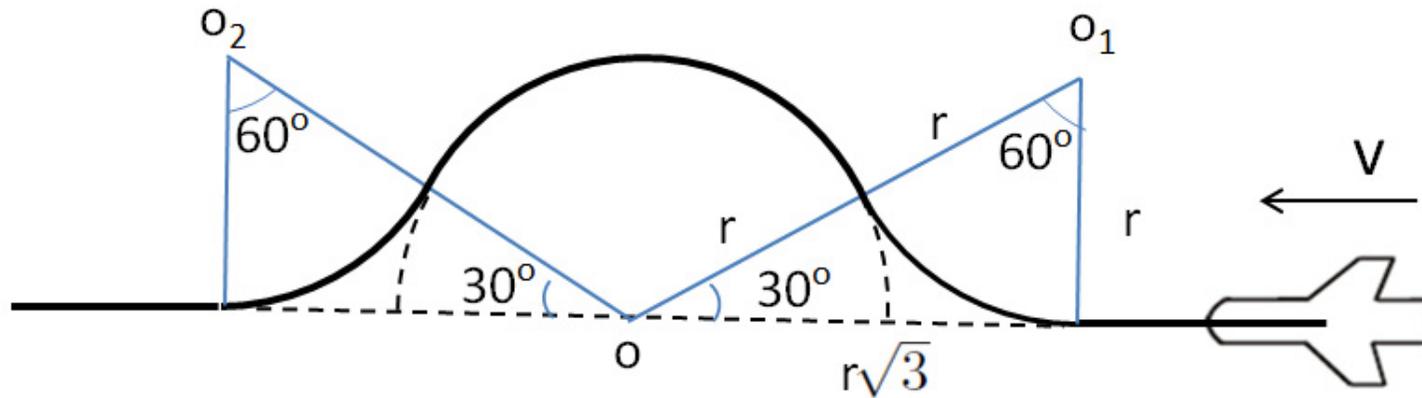




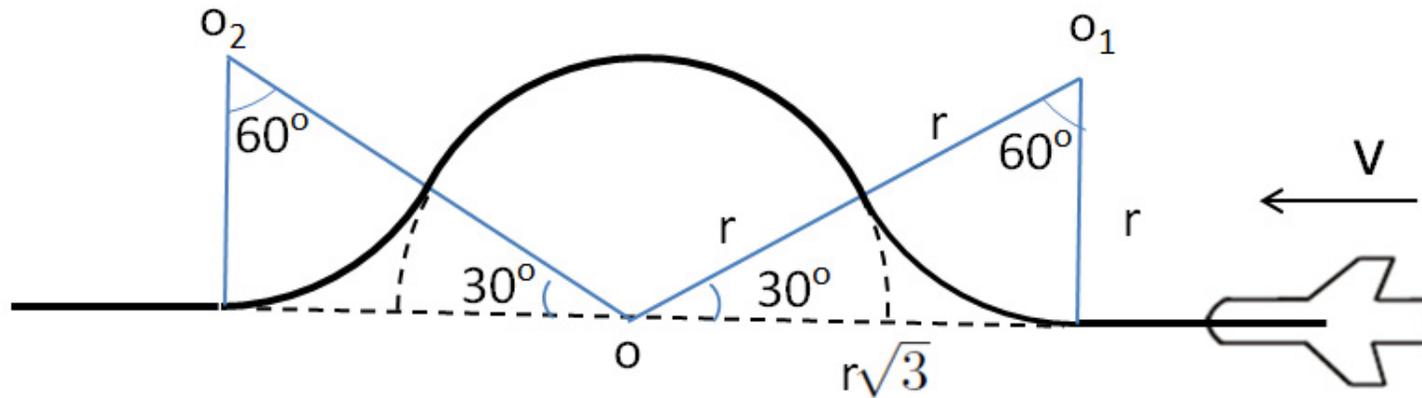
- Both aircraft fly as indicated on this figure



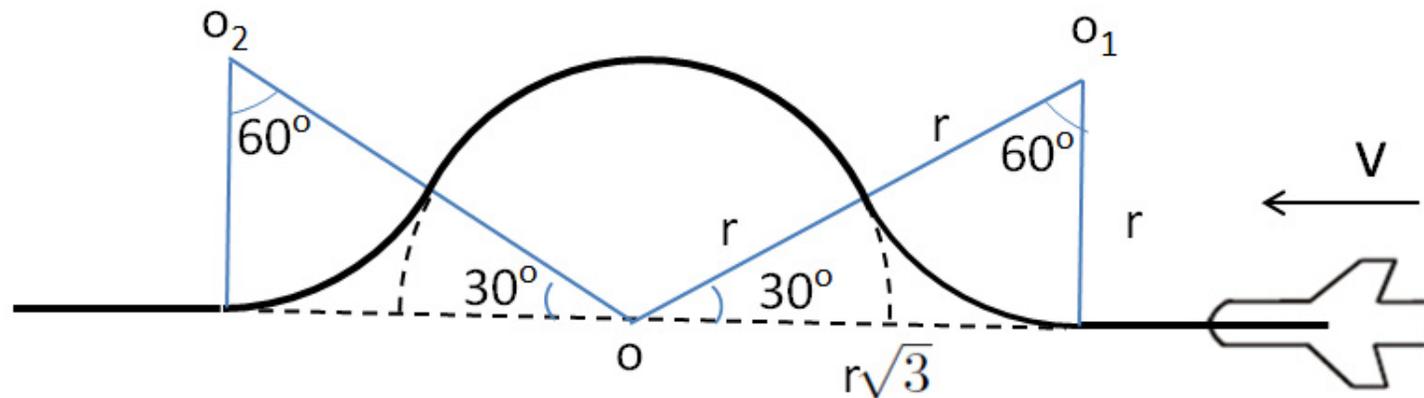
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- We have then:

$$\frac{p}{2 \sin \frac{\phi}{2}} \leq r \leq \frac{\rho_i}{\sqrt{3}}$$

- Here is again the possible interval for the radius r of the circle:

$$\frac{p}{2 \sin \frac{\phi}{2}} \leq r \leq \frac{\rho_i}{\sqrt{3}}$$

- We must have then the following for the constants ρ_i , ϕ , and p :

$$2\rho_i \sin \frac{\phi}{2} \geq p\sqrt{3}$$

- ϕ is the angle of the two trajectories
- ρ_i is the initial distance of the two aircrafts to the collision point o
- p is the minimal safety distance between the two aircrafts

$$\mathbf{axm1:} \quad \phi \in 0 .. \pi$$

$$\mathbf{axm2:} \quad \rho_i \in \mathbb{R}^+$$

$$\mathbf{axm2:} \quad p \in \mathbb{R}^+$$

$$\mathbf{axm4:} \quad 2\rho_i \sin \frac{\phi}{2} \geq p\sqrt{3}$$

- In this initial model, we are **still discrete**

- *phase* corresponds to the various discrete events
- ρ is the common distance of the aircrafts to the collision point o
- r is the circle radius

$$\mathbf{inv1:} \quad \mathit{phase} \in \{0, 1, 2, 3, 4, 5\}$$

$$\mathbf{inv2:} \quad \rho \in \mathbb{R}^+$$

$$\mathbf{inv3:} \quad r \in \mathbb{R}^+$$

$$\mathbf{inv4:} \quad 2\rho \sin \frac{\phi}{2} \geq p$$

- **inv4** is the **safety** invariant: the minimal authorized distance is p

- **INIT**: initialisation
- **agree**: choose the radius of the circle
- **start**: start the maneuver
- **enter**: entering the circle
- **cycle**: move on the circle
- **leave**: leaving the circle

INIT

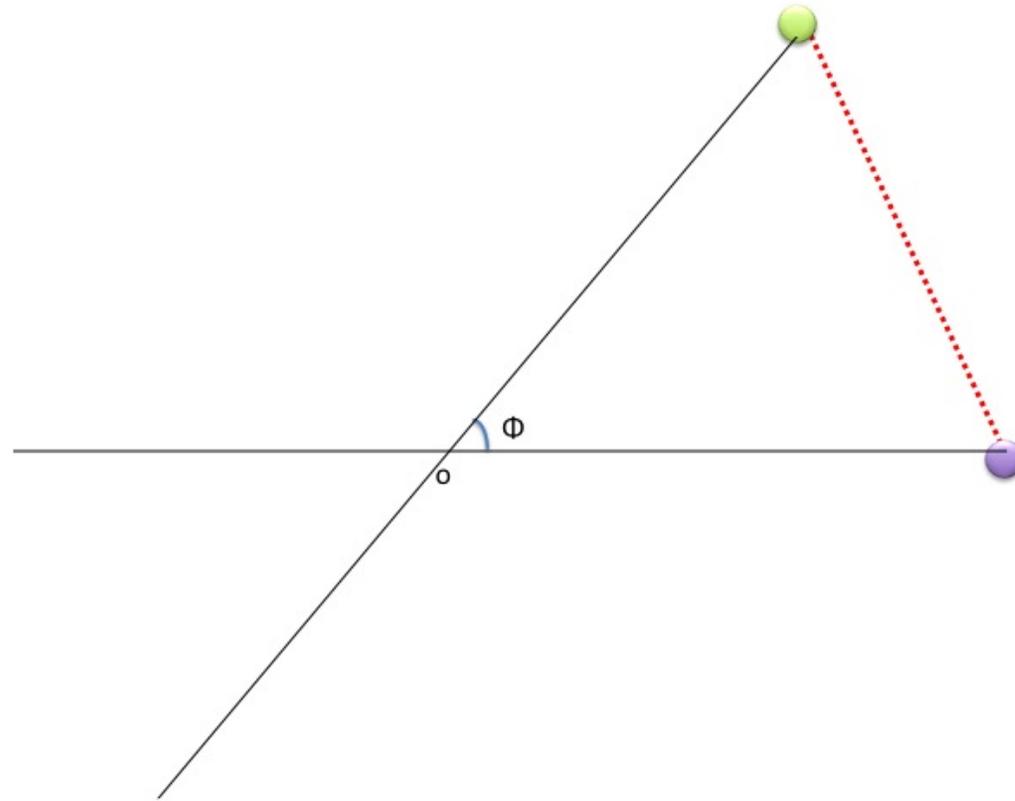
begin

$\rho := \rho_i$

$phase := 0$

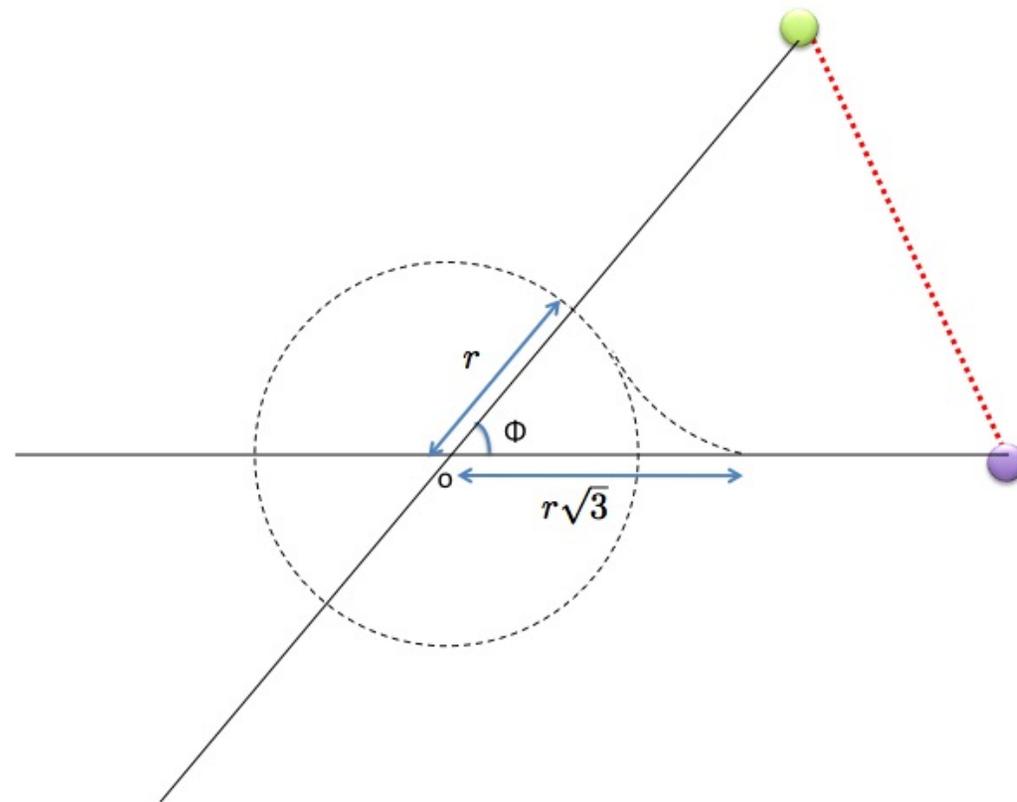
$r \in \mathbb{R}^+$

end



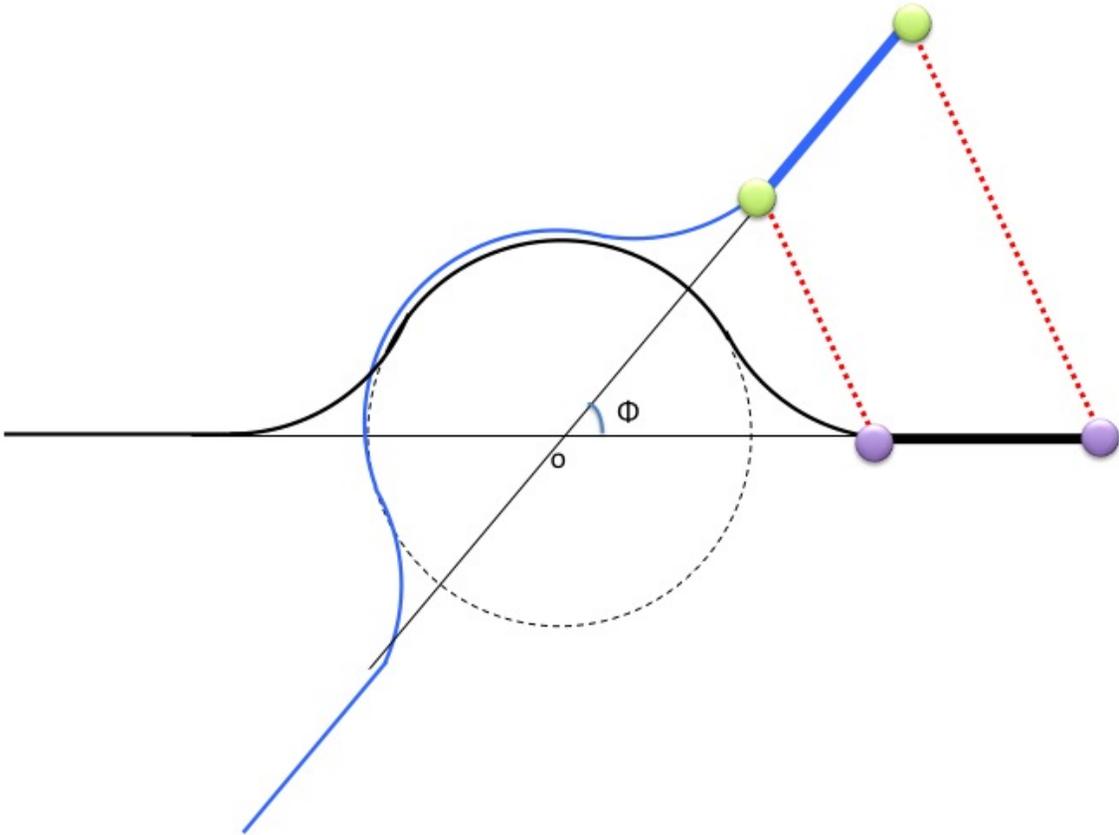
```
agree
  any  $c$  where
     $phase = 0$ 
     $p \leq 2c \sin \frac{\phi}{2}$ 
     $c\sqrt{3} \leq \rho_i$ 
  then
     $phase := 1$ 
     $r := c$ 
  end
```

Choosing the **radius r** of the circle



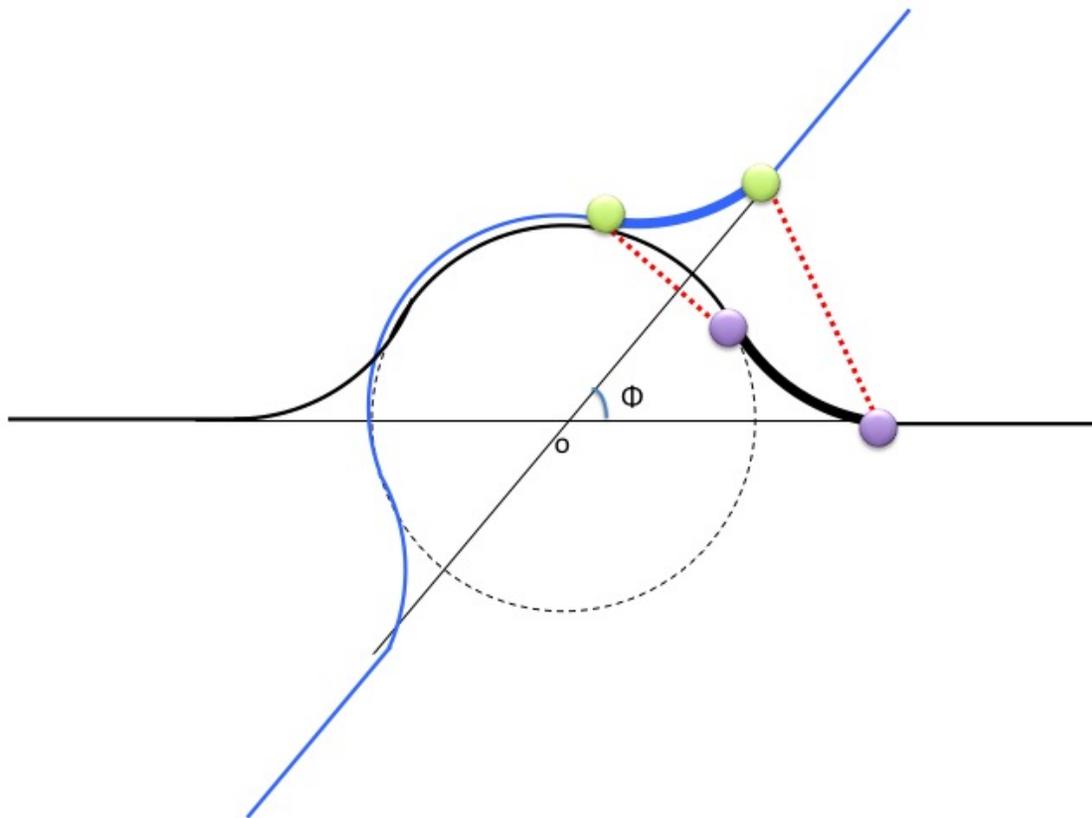
```
start
when
  phase = 1
then
  phase := 2
   $\rho := r\sqrt{3}$ 
end
```

ρ goes from ρ_i to $r\sqrt{3}$



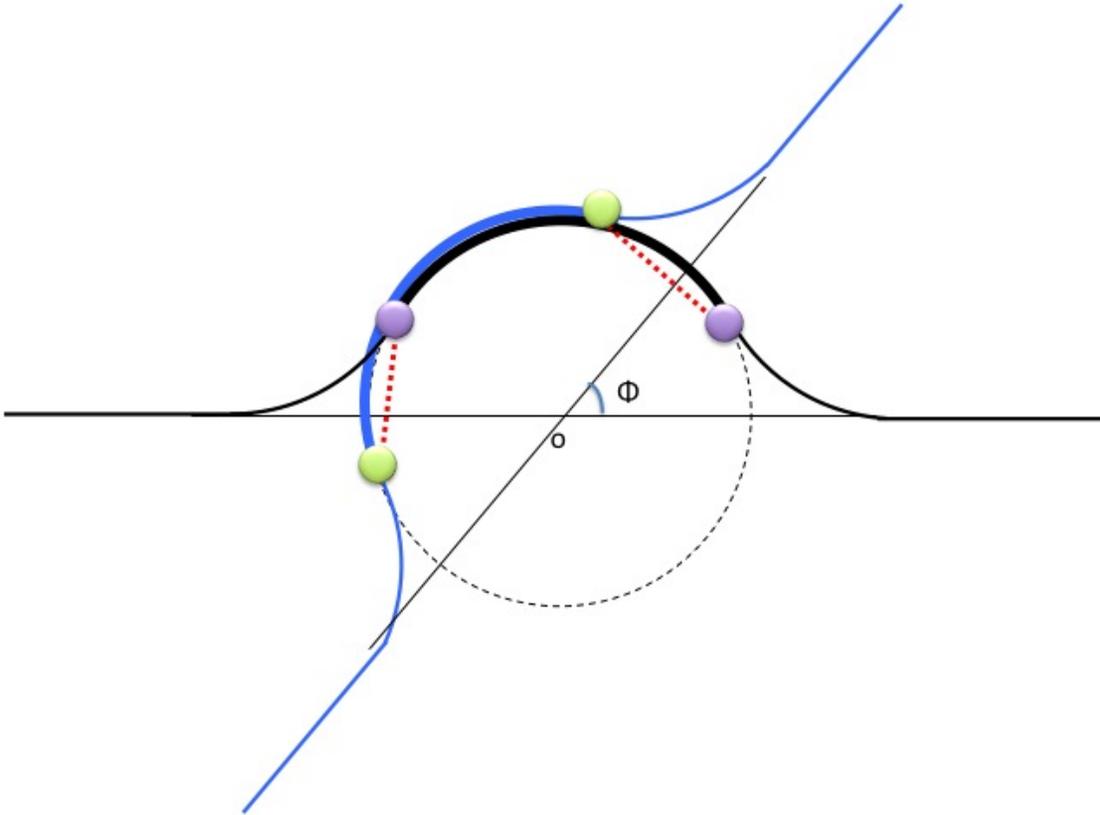
```
enter  
when  
   $phase = 2$   
then  
   $phase := 3$   
   $\rho := r$   
end
```

ρ goes from $r\sqrt{3}$ to r



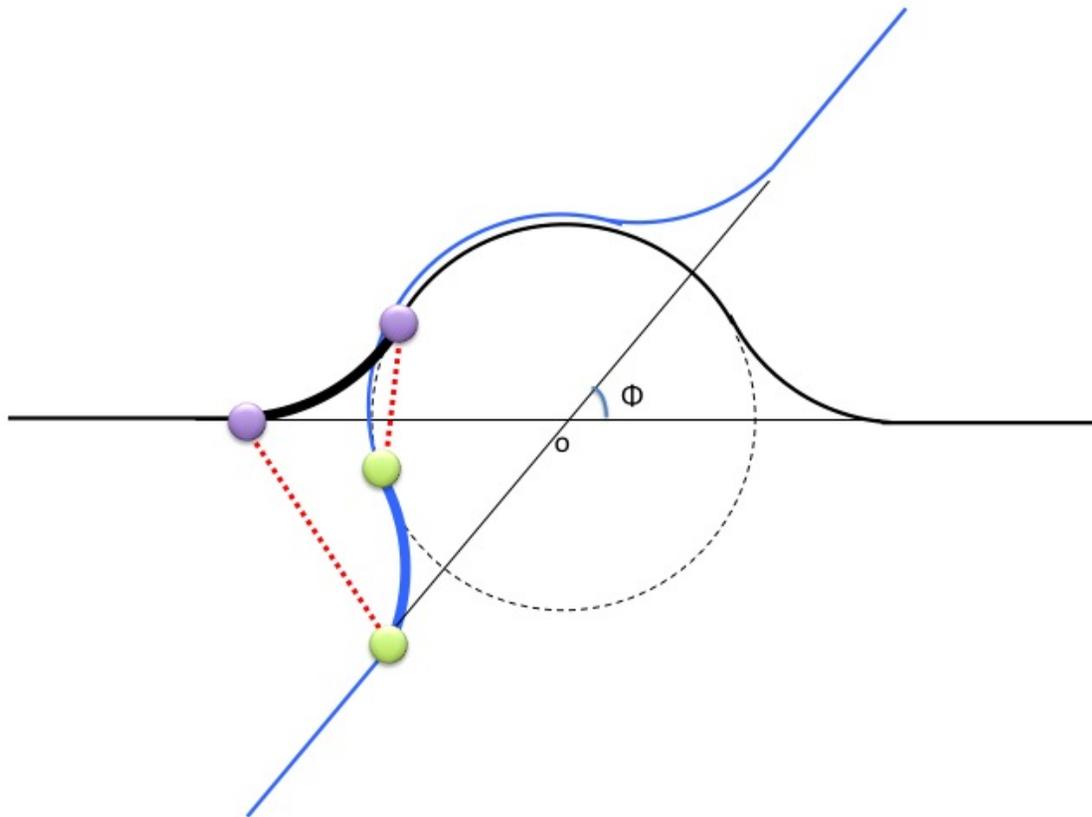
```
cycle
  when
    phase = 3
  then
    phase := 4
     $\rho := r$ 
  end
```

ρ goes from r to r



```
leave  
when  
   $phase = 4$   
then  
   $phase := 5$   
   $\rho := r\sqrt{3}$   
end
```

ρ goes from r to $r\sqrt{3}$



- We introduce the intermediate **continuous** parts
- We replace ρ by ρ_c (that is ρ_c *continuous*)
- We introduce *now*, the **present time**

$$\text{inv1_1: } \rho_c \in \mathbb{R}^+ \rightarrow \mathbb{R}$$

$$\text{inv1_2: } \textit{now} \in \text{dom}(\rho_c)$$

$$\text{inv1_3: } \rho = \rho_c(\textit{now})$$

$$\text{inv1_4: } \forall t \cdot t \in \text{dom}(\rho_c) \Rightarrow 2\rho_c(t) \sin \frac{\phi}{2} \geq p$$

- **inv1_3** is the **gluing invariant**
- **inv1_4** generalises the previous invariant: $2\rho \sin \frac{\phi}{2} \geq p$

(abstract-)INIT

begin

$\rho := \rho_i$

$phase := 0$

$r \in \mathbb{R}^+$

end

(concrete-)INIT

begin

$\rho_c := \{0 \mapsto \rho_i\}$

$phase := 0$

$r \in \mathbb{R}^+$

$now := 0$

end

agree

any c **where**

$phase = 0$

$p \leq 2c \sin \frac{\phi}{2}$

$c\sqrt{3} \leq \rho_i$

then

$phase := 1$

$r := c$

end

(abstract-)start

when

$phase = 1$

then

$phase := 2$

$\rho := r\sqrt{3}$

end

(concrete-)start

when

$phase = 1$

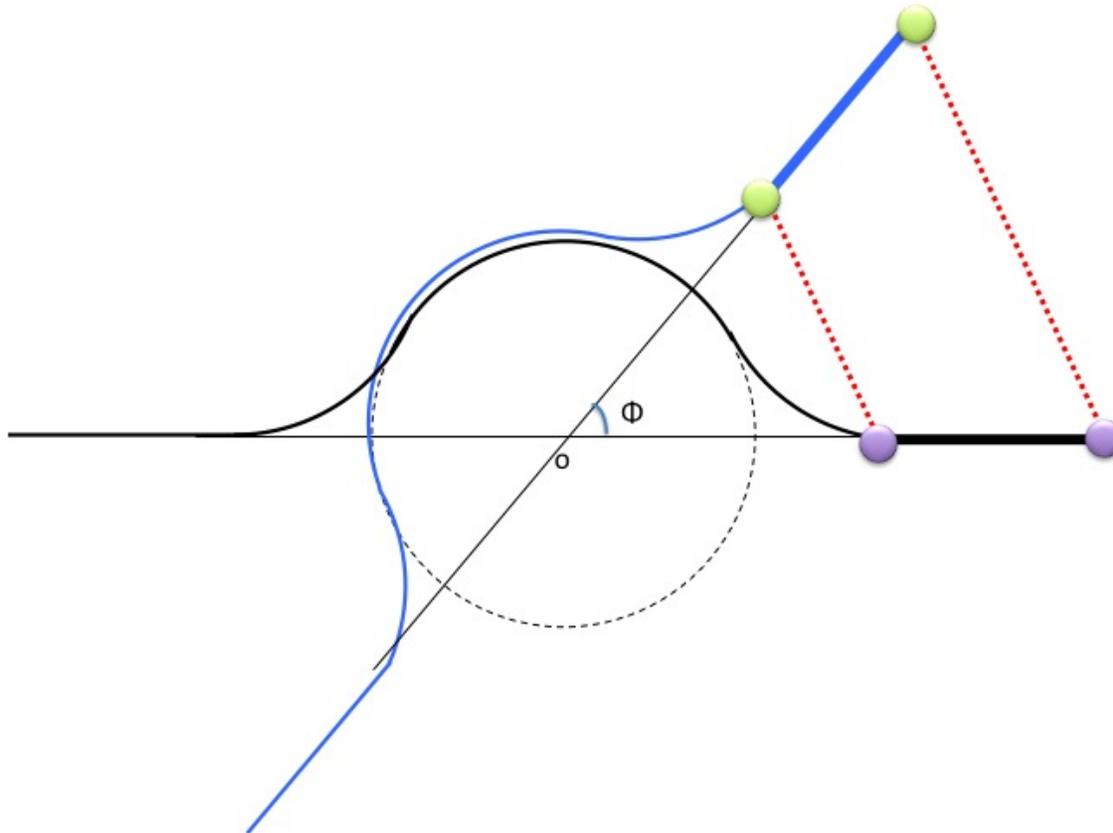
then

$phase := 2$

$\rho_c := \lambda t \cdot t \in now .. now + \frac{(\rho_i - r\sqrt{3})}{v} \mid \rho_i - v(t - now)$

$now := now + \frac{(\rho_i - r\sqrt{3})}{v}$

end



start

when

$phase = 1$

then

$phase := 2$

$\rho_c := \lambda t \cdot t \in now .. now + \frac{(\rho_i - r\sqrt{3})}{v} \mid \rho_i - v(t - now)$

$now := now + \frac{(\rho_i - r\sqrt{3})}{v}$

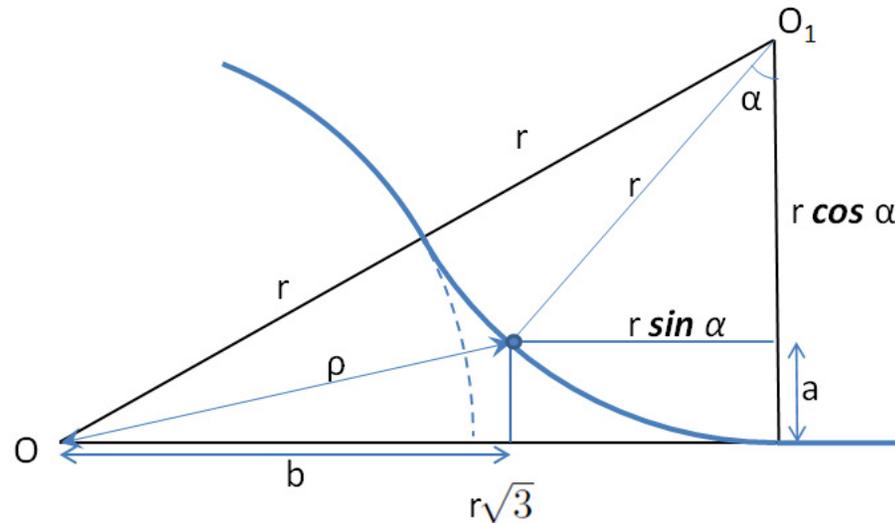
end

- $\rho_c(now) = \rho_i$

- $\rho_c(now + \frac{(\rho_i - r\sqrt{3})}{v}) = r\sqrt{3}$

- ρ_c decreases linearly from ρ_i to $r\sqrt{3}$

- $\frac{(\rho_i - r\sqrt{3})}{v}$ is the time it takes to fly from ρ_i to $r\sqrt{3}$



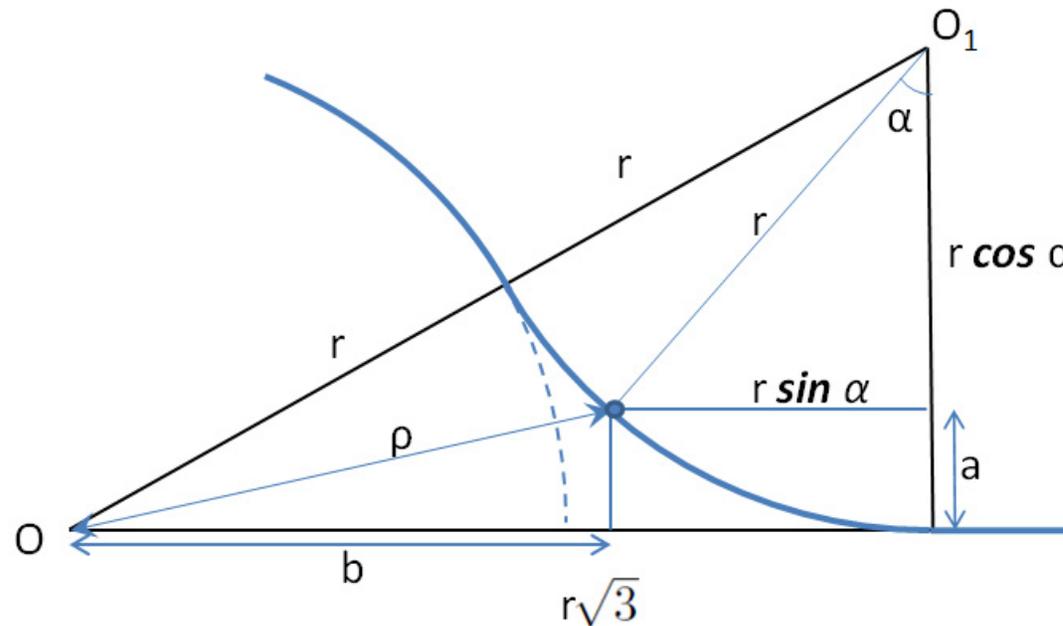
$$\rho^2 = a^2 + b^2$$

$$= r^2(1 - \cos \alpha)^2 + r^2(\sqrt{3} - \sin \alpha)^2$$

$$= r^2(5 - 4 \cos(\frac{\pi}{3} - \alpha))$$

$$\rho = r \sqrt{5 - 4 \cos(\frac{\pi}{3} - \alpha)}$$

- ρ decreases from $r\sqrt{3}$ to r when α goes from 0 to $\frac{\pi}{3}$.



- The angle α increases from 0 to $\frac{\pi}{3}$ during this phase
- The distance is $\frac{\pi r}{3}$
- The time to cover this distance is thus $\frac{\pi r}{3v}$
- We have: $\alpha = \frac{v(t-now)}{r}$

```

(abstract-)enter
  when
    phase = 2
  then
    phase := 3
    ρ := r
  end

```

```

(concrete-)enter

```

```

  when

```

```

    phase = 2

```

```

  then

```

```

    phase := 3

```

```

    ρ_c := λ t · t ∈ now .. now +  $\frac{\pi r}{3v}$  |  $r \sqrt{5 - 4 \cos\left(\frac{\pi}{3} - \frac{v(t-now)}{r}\right)}$ 

```

```

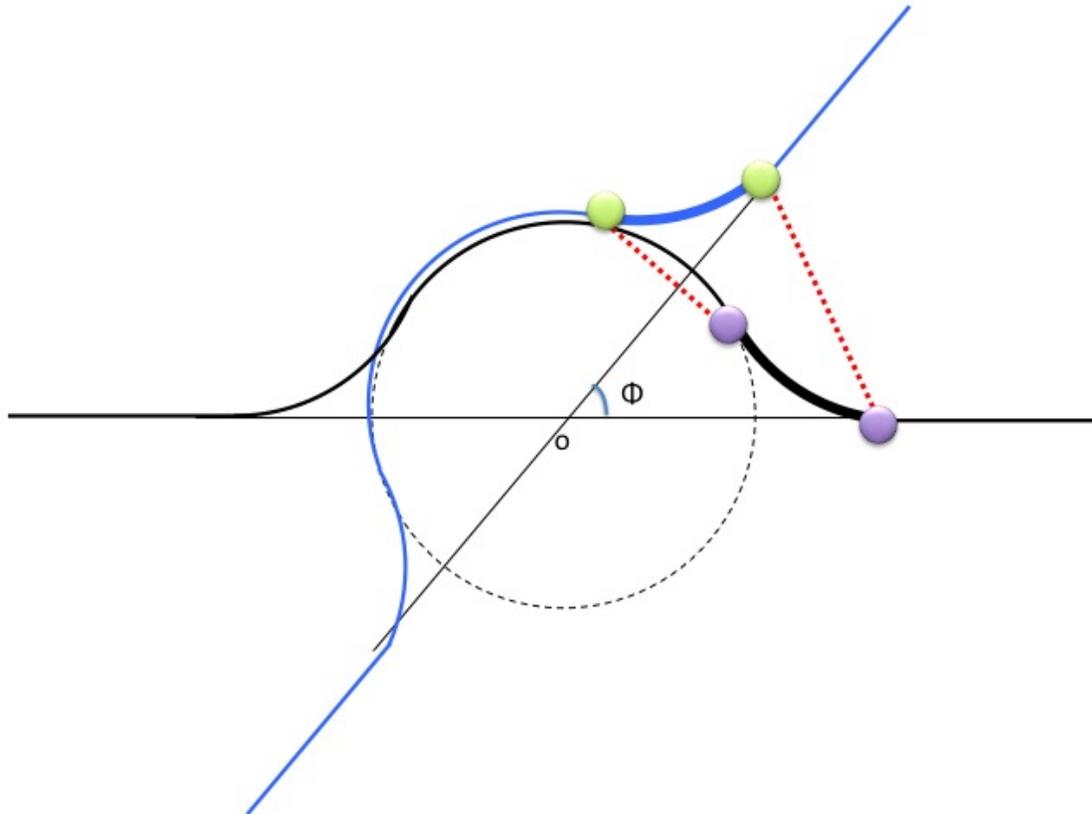
    now := now +  $\frac{\pi r}{3v}$ 

```

```

  end

```



```
enter
```

```
  when
```

```
    phase = 2
```

```
  then
```

```
    phase := 3
```

```
     $\rho_c := \lambda t \cdot t \in \text{now} .. \text{now} + \frac{\pi r}{3v} \mid r \sqrt{5 - 4 \cos\left(\frac{\pi}{3} - \frac{v(t-\text{now})}{r}\right)}$ 
```

```
    now := now +  $\frac{\pi r}{3v}$ 
```

```
  end
```

$$- \rho_c(\text{now}) = r \sqrt{5 - 4 \cos \frac{\pi}{3}} = r \sqrt{5 - \frac{4}{2}} = r\sqrt{3}$$

$$- \rho_c\left(\text{now} + \frac{\pi r}{3v}\right) = r \sqrt{5 - 4 \cos\left(\frac{\pi}{3} - \frac{v\pi r}{r3v}\right)} = r \sqrt{5 - 4 \cos 0} = r$$

- ρ_c decreases non-linearly from $r\sqrt{3}$ to r

$$\rho_c(t) = r \sqrt{5 - 4 \cos\left(\frac{\pi}{3} - \frac{v(t - \text{now})}{r}\right)}$$

Thus

$$\frac{d\rho_c(t)}{dt} = \frac{4r \sin\left(\frac{\pi}{3} - \frac{v(t - \text{now})}{r}\right) \cdot (-v)}{2\sqrt{5 - 4 \cos\left(\frac{\pi}{3} - \frac{v(t - \text{now})}{r}\right)}} \cdot r$$

When t increases from now to $\text{now} + \frac{\pi r}{3v}$, then the derivative

$\frac{d\rho_c(t)}{dt}$ increases **monotonically** from $-v$ to 0 :

$$\frac{d\rho_c(t)}{dt} \Big|_{t=\text{now}} = -v$$

$$\frac{d\rho_c(t)}{dt} \Big|_{t=\text{now} + \frac{\pi r}{3v}} = 0$$

(abstract-)cycle

when

$phase = 3$

then

$phase := 4$

$\rho := r$

end

(concrete-)cycle

when

$phase = 3$

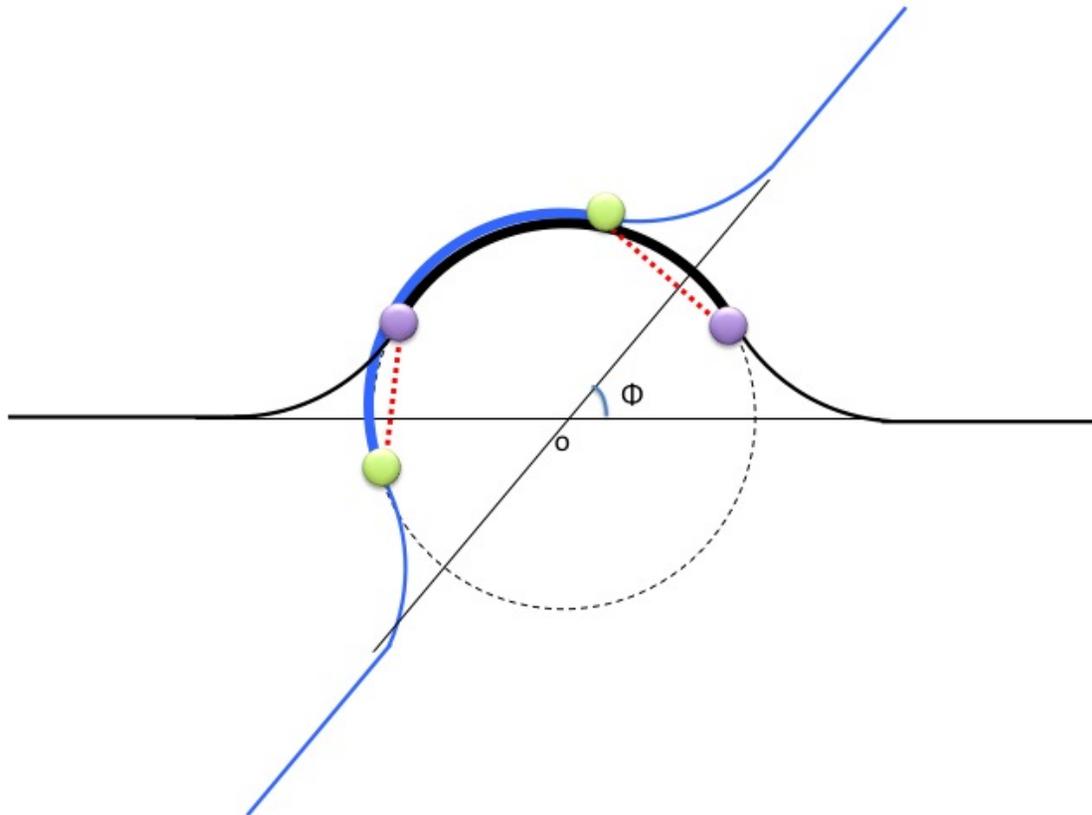
then

$phase := 4$

$\rho_c := \lambda t \cdot t \in now .. now + \frac{2\pi r}{3v} \mid r$

$now := now + \frac{2\pi r}{3v}$

end



```
cycle
  when
    phase = 3
  then
    phase := 4
     $\rho_c := \lambda t \cdot t \in \text{now} .. \text{now} + \frac{2\pi r}{3v} \mid r$ 
     $\text{now} := \text{now} + \frac{2\pi r}{3v}$ 
  end
```

- $\rho_c(\text{now}) = r$

- $\rho_c(\text{now} + \frac{2\pi r}{3v}) = r$

- ρ_c remains constant to r

(abstract-)leave

when

$phase = 4$

then

$phase := 5$

$\rho := r\sqrt{3}$

end

(concrete-)leave

when

$phase = 4$

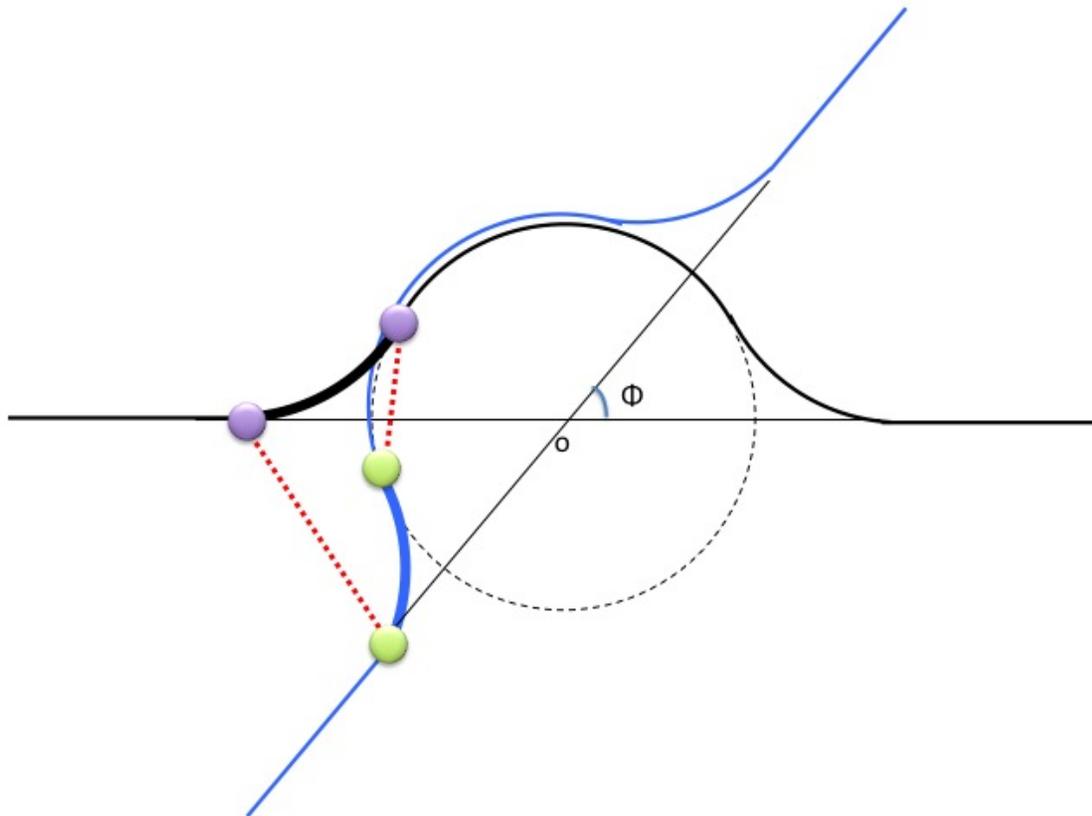
then

$phase := 5$

$\rho_c := \lambda t \cdot t \in now .. now + \frac{\pi r}{3v} \mid r \sqrt{5 - 4 \cos\left(\frac{v(t-now)}{r}\right)}$

$now := now + \frac{\pi r}{3v}$

end



leave

when

$phase = 4$

then

$phase := 5$

$\rho_c := \lambda t \cdot t \in now .. now + \frac{\pi r}{3v} \mid r \sqrt{5 - 4 \cos\left(\frac{v(t-now)}{r}\right)}$

$now := now + \frac{\pi r}{3v}$

end

- $\rho_c(now) = r \sqrt{5 - 4 \cos 0} = r$

- $\rho_c\left(now + \frac{\pi r}{3v}\right) = r \sqrt{5 - 4 \cos \frac{\pi}{3}} = r \sqrt{5 - \frac{4}{2}} = r \sqrt{3}$

- ρ_c increases non-linearly from r to $r \sqrt{3}$

$$\rho_c(t) = r \sqrt{5 - 4 \cos\left(\frac{v(t - \text{now})}{r}\right)}$$

Thus

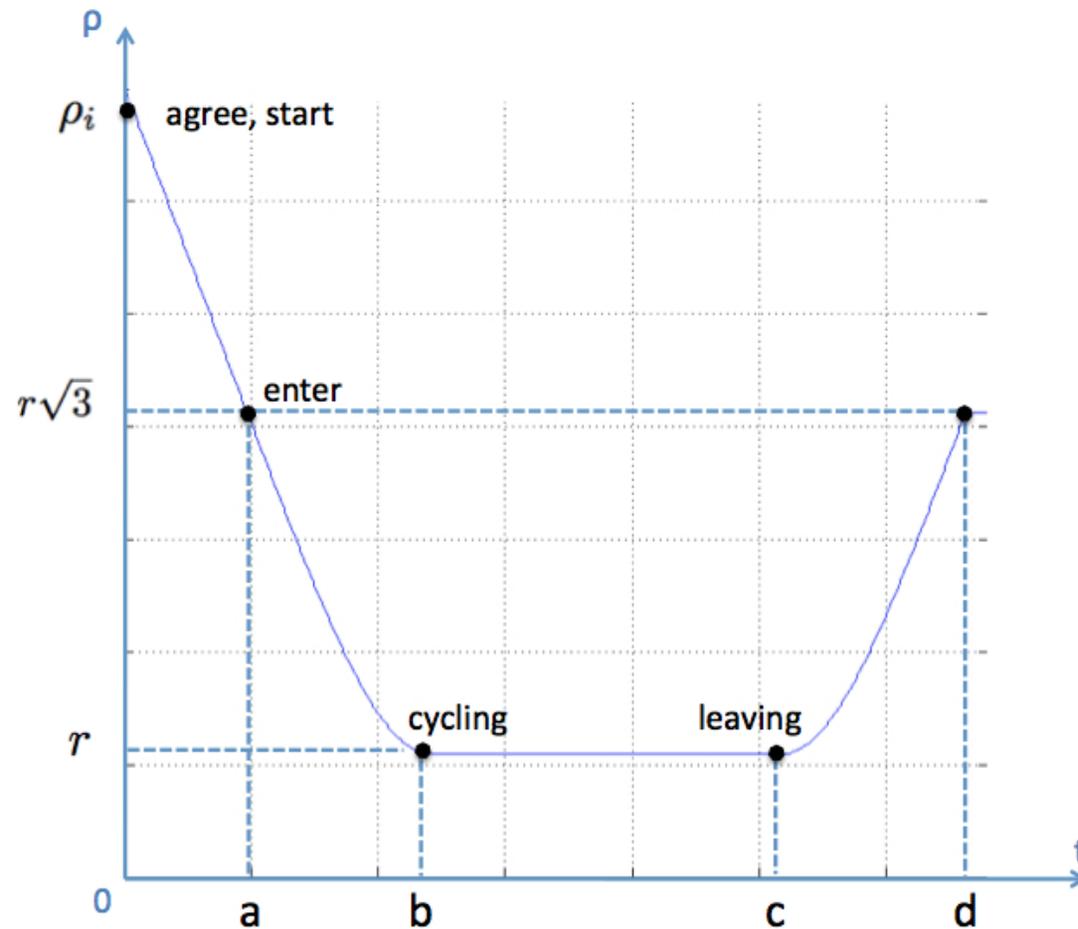
$$\frac{d\rho_c(t)}{dt} = \frac{4r \sin\left(\frac{v(t - \text{now})}{r}\right) v}{2 \sqrt{5 - 4 \cos\left(\frac{v(t - \text{now})}{r}\right)} r}$$

When t increases from now to $\text{now} + \frac{\pi r}{3v}$, then the derivative

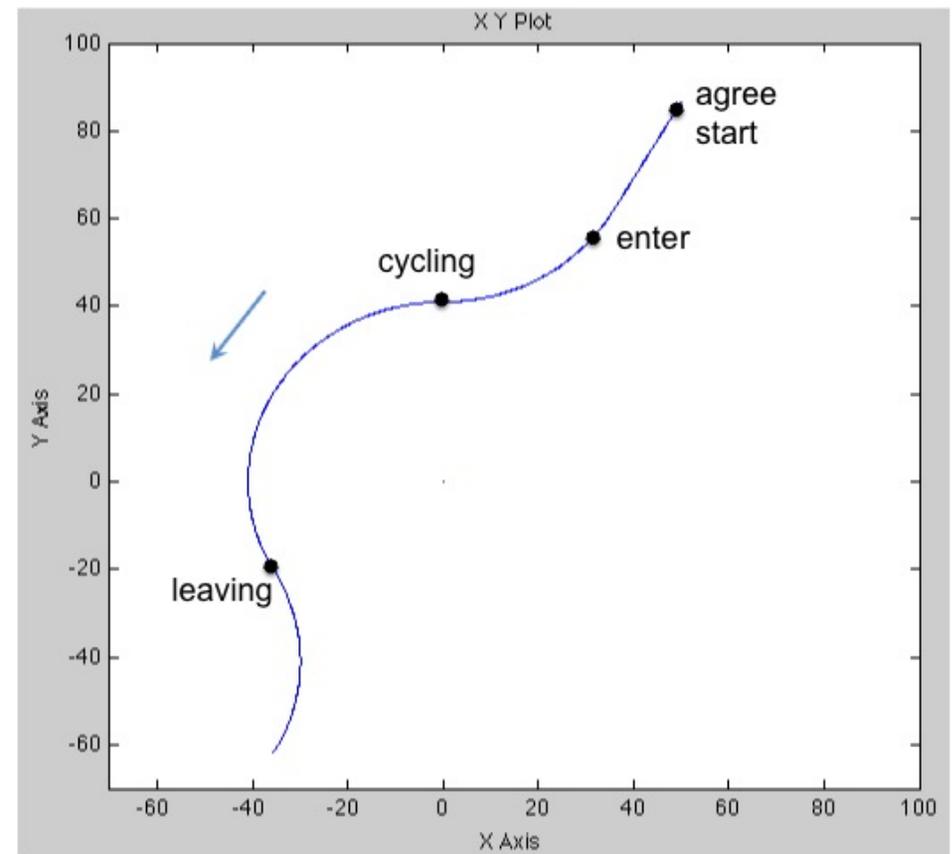
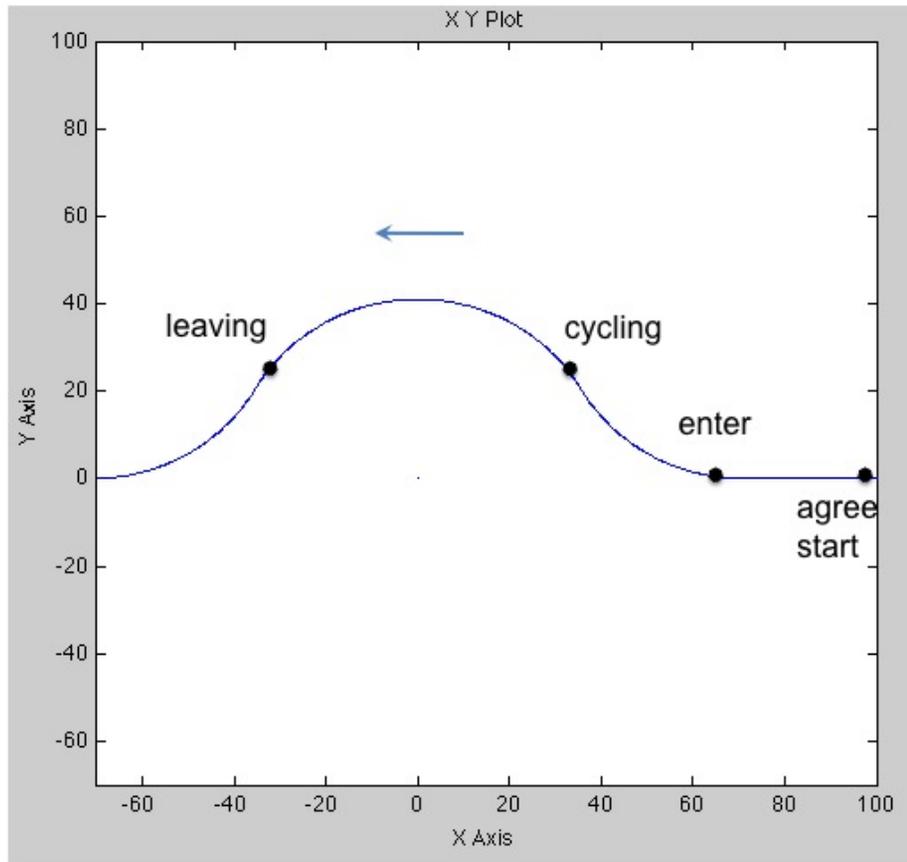
$\frac{d\rho_c(t)}{dt}$ increases **monotonically** from **0** to **v**:

$$\frac{d\rho_c(t)}{dt} \Big|_{t=\text{now}} = 0$$

$$\frac{d\rho_c(t)}{dt} \Big|_{t=\text{now} + \frac{\pi r}{3v}} = v$$



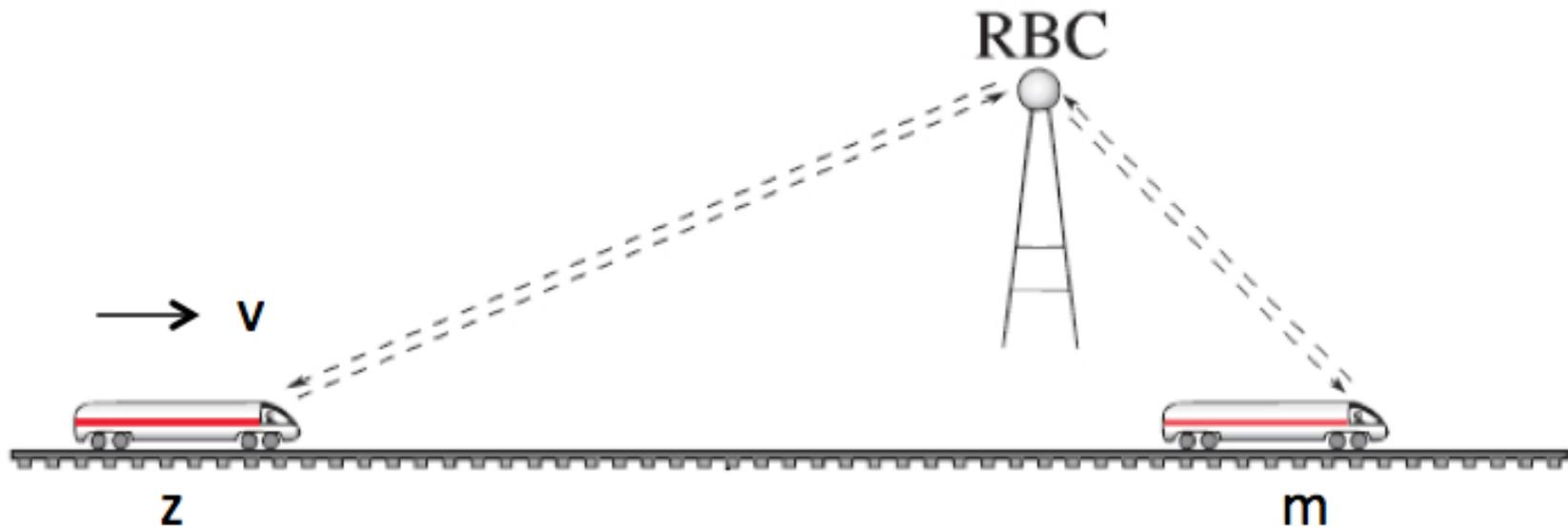
$$a = \frac{\rho_i - r\sqrt{3}}{v}, \quad b = a + \frac{\pi r}{3v}, \quad c = b + \frac{2\pi r}{3v}, \quad d = c + \frac{\pi r}{3v}$$



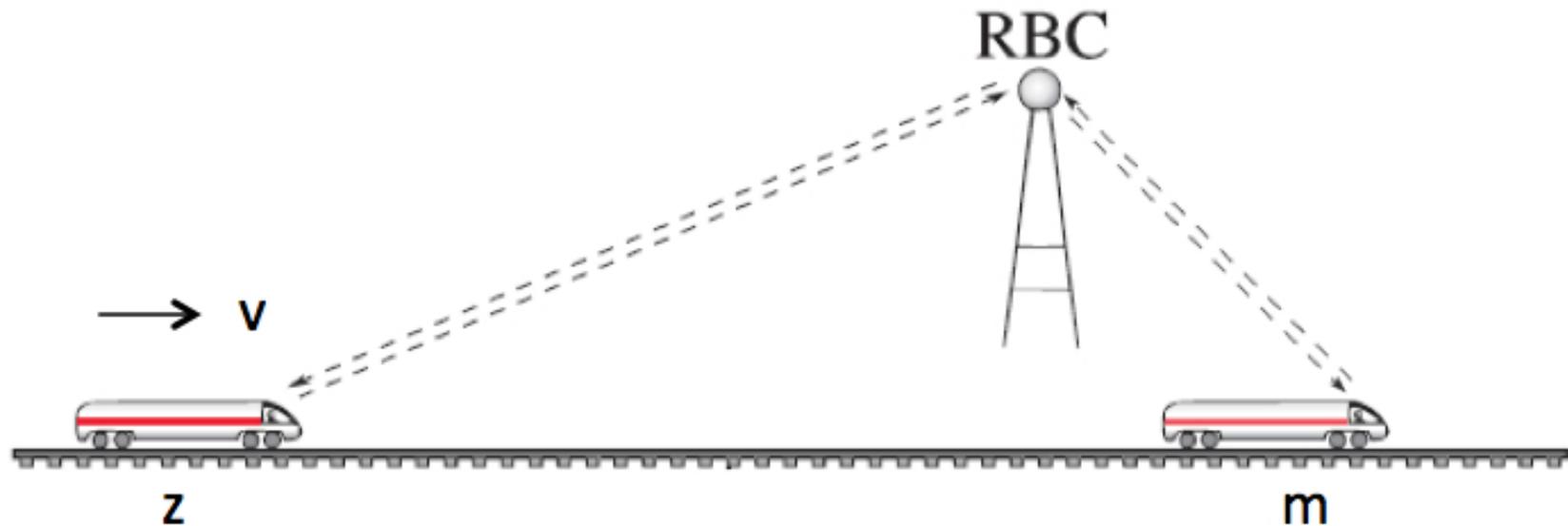
Example 2

- **Two trains** are sent some information by **R**adio **B**road**C**asting

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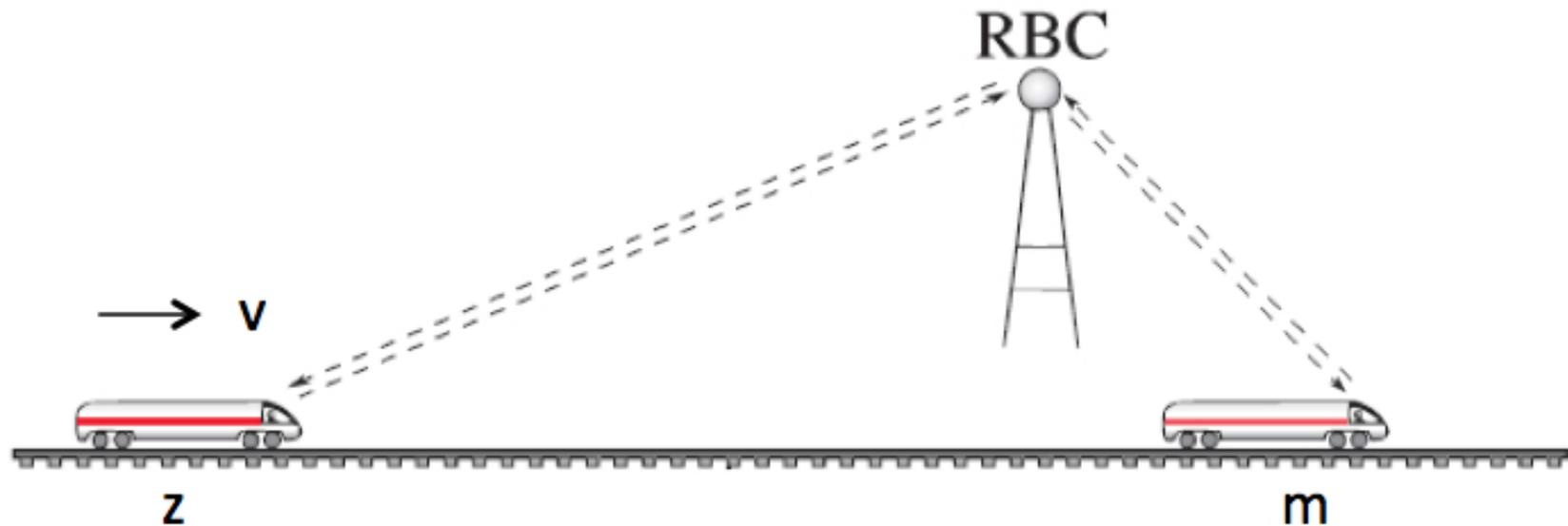


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- The **second train** is in position z

- **Two trains** are sent some information by **R**adio **B**road**C**asting



- The **second train** is in position z
- It is made aware of a position m where it should at the latest **stop**

- The **controller** in the **second train** reacts every other **ϵ seconds**

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- It can change the **acceleration** of the train according to **3 values**:
Accelerations are: A , $-b$, or 0 , where A and b are **positive**

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Accelerations are: A , $-b$, or 0 , where A and b are **positive**
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- The train should **never go backwards**
- **Goal**: Calculate the **best acceleration** at each controller's reaction.

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- This is the **main invariant** to be maintained

- At each control time (every other ϵ seconds), the invariant to be maintained is:

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$$2b(m - z - v\epsilon - a\frac{\epsilon^2}{2}) \geq (v + a\epsilon)^2$$

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that is

$$2b(m - z) \geq v^2 + (a\epsilon^2 + 2v\epsilon)(a + b)$$

- We must have the following after ϵ seconds:

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- Otherwise, the acceleration should be $-b$ (braking), resulting in:

$$2b(m - z) \geq v^2$$

- After the choice of acceleration, A or $-b$, the speed of the train is:

$$v + a\epsilon$$

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- If $v + a\epsilon > sl$, we must choose a 0 acceleration (instead of A)
- We have the additional invariant: $v \in 0 .. sl$
- We have thus three different controller decisions:
 - decision 1: acceleration $-b$
 - decision 2: acceleration A
 - decision 3: acceleration 0

- If the speed and position are v and z , then after ϵ seconds:

-
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 - the new speed of the train will be:
 - drive 1: if $v + a\epsilon \geq 0$ then $v + a\epsilon$
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 - the **new speed** of the train will be:
 - drive 1: if $v + a\epsilon \geq 0$ then $v + a\epsilon$
 - drive 2: if $v + a\epsilon < 0$ then 0
 - the **new position** of the train will be:
 - drive 1: if $v + a\epsilon \geq 0$ then $z + v\epsilon + a\frac{\epsilon^2}{2}$
 - drive 2: if $v + a\epsilon < 0$ then $z + \frac{v^2}{2b}$ (the train stops after time $\frac{v}{b}$)

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 - Continuous variables are **not** defined by **differential equations**

Thank you for listening